# HOWICK INNOVATION... READY TO ROLL 

## DESIGN CAPACITY TABLES

for
$64 \times 41$ Lipped Channels
to
AS/NZS 4600
Version 01
June 2019
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## Howick Ltd

Design Capacity Tables for 64 x 41 Lipped Channels to AS/NZS 4600
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## RELEVANCE OF INFORMATION CONTAINED IN THIS PUBLICATION:

Users of this publication should note that the design capacities, calculations, tabulations and other information contained in this publication are specifically relevant to cold-formed steel sections manufactured on Howick roll-forming machines.
Consequently, the information contained in this publication cannot be readily used for coldformed sections produced on machines by other manufacturers, as those sections may vary significantly in geometry and material Standard compliance.

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## About Howick Ltd

Howick Ltd is a well-established and respected, 35 year, family enterprise based in Auckland, New Zealand.

Howick Ltd personifies the concept of "Kiwi ingenuity" showcasing technical experties and creativity and that essential "can do" philosophy that underpins the company's world-leading innovation and quality. Given this success, Howick Ltd is often described as producers of "the world's best steel framing machines."

We are a design and manufacturing company with a global philosophy and reach. Our emphasis is on unique research and development and sophisticated design technology enabling cost-effective, efficient end to end construction systems, across a variety of steel framed projects.

## Notations \& Abbreviations

| Symbol |  |
| :---: | :--- |
| $A_{\mathrm{g}}$ | gross area of a cross-section |
| $b$ | flat width of a flange excluding radii |
| $b_{\mathrm{f}}$ | overall width of a flange |
| $C_{\mathrm{b}}$ | bending coefficient dependent on moment |
| $C_{\mathrm{s}}$ | coefficient for moment about the cnetroidal axis perpendicular to the <br> symmetry axis |
| $C_{\text {TF }}$ | coefficient for unequal end moment |
| $c$ | distance from the end of a beam to the edge of the bearing force |
| $d$ | overall depth of a section |
| $d_{\mathrm{l}}$ | depth of the flat portion of a web measured along the plane of the web |
| $d_{\mathrm{L}}$ | overall depth of a lip |
| $E$ | Young's modulus of elasticity |
| EOF | End One Flange (concentrated load or reaction on a beam) |
| ETF | End Two Flange (concentrated load or reaction on a beam) |
| $f_{\mathrm{u}}$ | minimum tensile strength used in design |
| $f_{\mathrm{y}}$ | minimum yield stress used in design |
| $G$ | shear modulus of elasticity |
| $I_{\mathrm{w}}$ | warping constant for a cross-section |
| $I_{\mathrm{x}}$ | second moment of area about the major principal x -axis |
| $I_{\mathrm{y}}$ | second moment of area about the minor principal y-axis |
| IOF $^{\text {ITF }}$ | Interior One Flange (concentrated load or reaction on a beam) |
| $J$ | Interior Two Flange (concentrated load or reaction on a beam) |
| $L_{\mathrm{b}}$ | torsion constant for the cross-section |
| $L_{\mathrm{e}}$ | actual length of bearing |
| $L_{\mathrm{ex}}$ | effective length of a member |
| $L_{\mathrm{ey}}$ | effective length for buckling about the major principal x-axis |
| $L_{\mathrm{ez}}$ | effective length for buckling about the minor principal y-axis length for torsional buckling about the longitudinal z-axis |
| $M^{*}$ | design bending moment |


| Symbol | Description |
| :---: | :---: |
| $M_{\text {x }}{ }^{*}$ | design bending moment about the x -axis |
| $M_{\text {y }}{ }^{*}$ | design bending moment about the y -axis |
| $M_{\text {b }}$ | nominal member moment capacity |
| $M_{\text {bdx }}$ | nominal moment capacity about the $x$-axis for distortional buckling |
| $M_{\text {bdyL }}$ | nominal moment capacity about the $y$-axis for distortional buckling (lips in compression) |
| $M_{\text {bdy }}$ | nominal moment capacity about the $y$-axis for distortional buckling (web in compression) |
| $M_{\text {bx }}$ | nominal member moment capacity about the $x$-axis |
| $M_{\text {by }}$ | nominal member moment capacity about the $y$-axis |
| $M_{\text {byL }}$ | nominal member moment capacity about the y -axis (lips in compression) |
| $M_{\text {byw }}$ | nominal member moment capacity about the $y$-axis (web in compression) |
| $M_{\text {sx }}$ | nominal section moment capacity about the $x$-axis |
| $M_{\text {sxf }}$ | nominal yield moment capacity about the $x$-axis |
| $M_{\text {syft }}$ | nominal yield moment capacity about the $y$-axis (tension in the lips) |
| $M_{\text {syfT }}$ | nominal yield moment capacity about the y -axis (tension in the toes) |
| $M_{\text {syyw }}$ | nominal yield moment capacity about the y-axis (tension in the web) |
| $M_{\text {syL }}$ | nominal section moment capacity about the y-axis (lips in compression) |
| $M_{\text {syT }}$ | nominal section moment capacity about the y -axis (toes in compression) |
| $M_{\text {syw }}$ | nominal section moment capacity about the y-axis (web in compression) |
| $M_{y}$ | moment causing initial yield at the extreme compression fibre of a full section |
| $N^{*}$ | design axial force (tension or compression) |
| $N_{\text {c }}$ | nominal member capacity of a member in compression |
| $N_{\text {cd }}$ | nominal capacity of a member in compression for distortional buckling |
| $N_{\text {ex }}$ | elastic buckling load about the major principal x -axis |
| $N_{\text {ey }}$ | elastic buckling load about the minor principal $y$-axis |
| $N_{\text {s }}$ | nominal section capacity of a member in compression |
| $N_{\text {t }}$ | nominal section capacity of a member in tension |


| Symbol |  |
| :---: | :--- |
| $r_{\mathrm{i}}$ | inside corner radius |
| $r_{01}$ | polar radius of gyration of the cross-section about the shear centre |
| $r_{\mathrm{x}}$ | radius of gyration about the major principal x -axis |
| $r_{\mathrm{y}}$ | radius of gyration about the minor principal y -axis |
| $t$ | nominal base metal thickness of a section exclusive of coatings |
| $V_{\mathrm{vx}}$ | nominal shear capacity of the cross-section perpendicular to the x -axis |
| $V_{\mathrm{vy}}$ | nominal shear capacity of the cross-section perpendicular to the x -axis |
| $V_{\mathrm{x}}{ }^{*}$ | design shear force |
| $V_{\mathrm{y}}{ }^{*}$ | design shear force |
| $w_{\mathrm{h}}$ | total hole width |
| $x$ | major principal axis of the cross-section |
| $x_{\mathrm{c}}$ | co-ordinate of the centroid from the back of the web along the x -axis |
| $x_{\mathrm{o}}$ | co-ordinate of the shear centre from the centroid along the x -axis |
| $y$ | minor principal axis of the cross-section |
| $Z_{\mathrm{x}}$ | elastic section modulus about the major principal x -axis |
| $z_{\mathrm{y} L}$ | elastic section modulus about the minor principal y -axis <br> (lips in compression) |
| $z_{\mathrm{yw}}$ | elastic section modulus about the minor principal y -axis <br> (web in compression) |
| $\alpha_{\mathrm{T}}$ | coefficient of thermal expamsion |
| $\beta_{\mathrm{y}}$ | monosymmetry section constant about the y -axis |
| $\phi_{\mathrm{b}}$ | capacity reduction factor for bending |
| $\phi_{\mathrm{c}}$ | capacity reduction factor for compression |
| $\phi_{\mathrm{t}}$ | capacity reduction factor for tension |
| $\phi_{\mathrm{v}}$ | capacity reduction factor for shear |
| $\phi_{\mathrm{w}}$ | capacity reduction factor for bearing |
| $v$ | Poisson's ratio (= 0.3 for steel) |
| $\rho$ | density of steel |

## INTRODUCTION

## Scope

These Design Capacity Tables have been prepared for the following nestable lipped channel cold-formed sections manufactured on Howick Ltd. steel roll-forming machines.

$$
\begin{aligned}
& 64 \times 41 \times 1.55 L C \\
& 64 \times 41 \times 1.15 L C \\
& 64 \times 41 \times 0.95 L C \\
& 64 \times 41 \times 0.75 L C
\end{aligned}
$$

The values presented in the tables and graphs are only applicable to sections manufactured on Howick Ltd. machines, and for the specified steel grades complying with AS 1397.

All of the dimensions and section properties required for design are provided, as well as design aids in the form of tables and graphs for members subject to the following design actions:

## Bending

Axial Compression
Axial Tension
Combined Actions
These design aids will allow engineers to design most structures without having to refer to the design standard AS/NZS 4600.

## Design Method

The Tables and Graphs in this publication have been calculated generally in accordance with the Australian and New Zealand standard AS/NZS 4600 Cold-Formed steel Structures. The Direct Strength Method (DSM) has been used to determine the capacities for axial compression and bending, based on the results of finite strip analyses using the computer program "Thin-Wall" from The University of Sydney.

Where appropriate, the method of calculating capacities in the transition region between local and distortional buckling in accordance with the AISI publication "Direct Strength Mothod" has been used. This is an extension of what is given in AS/NZS 4600.

## Limit States Design

All values presented in these Design Capacity Tables are limit state values in accordance with the Limits State Design requirements of AS/NZS 4600 and AS/NZS 1170.0.

## Units

The units in the Tables are consistent with those in the SI (metric) system. The base units used in the tables and graphs are:

| Property | Units | Symbol |
| :---: | :---: | :---: |
| Force | Newton | N |
| Length | metre | m |
| Mass | kilogram | kg |
| Stress | Megapascal | MPa |

Except for some minor exceptions, all values in the Tables are rounded to three (3) significant figures.

## Properties of Steel

The properties of steel used for the calculation of capacities in these Tables are given in the table below. The coefficient of expansion for steel is also listed.

| Property | Symbol | Value |
| :--- | :---: | :---: |
| Young's Modulus of Elasticity | $E$ | $200 \times 10^{3} \mathrm{MPa}$ |
| Shear Modulus | G | $80 \times 10^{3} \mathrm{MPa}$ |
| Poisson's Ratio | $v$ | 0.3 |
| Density | $\rho$ | $7850 \mathrm{~kg} / \mathrm{m}^{3}$ |
| Coefficient of Thermal Expansion | $\alpha_{T}$ | $11.7 \times 10^{-6} \mathrm{per}{ }^{\circ} \mathrm{C}$ |

The steel grades and mechanical properties used for design in accordance with AS/NZS 4600 are given in the table below. Note that the yield stress and tensile strength for thin sections of Grade G550 steel are reduced as required by this standard.

| Section | Grade | Yield Stress <br> $f_{y}(M P a)$ | Tensile Strength <br> $f_{u}(M P a)$ |
| :---: | :---: | :---: | :---: |
| $64 \times 41 \times 1.55$ LC | G450 | 450 | 480 |
| $64 \times 41 \times 1.15$ LC | G500 | 500 | 520 |
| $64 \times 41 \times 0.95$ LC | G550 | 550 | 550 |
| $64 \times 41 \times 0.75$ LC | G550 | 495 | 495 |

## References

Referenced Standards
AS 1397-2011, Continuous hot-dip metallic coated steel sheet and strip - Coatings of zinc and zinc alloyed with aluminium and magnesium, Standards Australia

AS/NZS 1170.1: 2002, Structural Design Actions Part 0: General Principles, Standards
Australia.
AS/NZS 4600: 2018, Cold-Formed Steel Structures, Standards Australia.
Other References
AISI 2006, Direct Strength Method (DSM) Design Guide, American Iron and Steel Institute, January 2006.
Centre of Advanced Structural Engineering (CASE) 2001, "THIN-WALL", Computer Program.

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## Part 1: <br> Dimensions \& Section Properties



## Table 1.1

## DIMENSIONS \& SECTION PROPERTIES



| DIMENSIONS |  |  |  |  |  |  |  | SECTION PROPERTIES |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Designation | Depth <br> d | Flange Width $b_{\text {f }}$ | Lip Depth $d_{\mathrm{L}}$ | Thick. <br> $t$ | Inside <br> Corner <br> Radius <br> $r_{i}$ | $\begin{gathered} \text { Co-ord. } \\ \text { of } \\ \text { Centroid } \\ x_{\mathrm{c}} \end{gathered}$ | Mass per metre | Gross <br> Section <br> Area <br> $A_{g}$ | About $x$-axis |  |  | About $y$-axis |  |  |  |
|  | mm | mm | mm | mm | mm | mm | kg/m | $\mathrm{mm}^{2}$ | $10^{6} \mathrm{~mm}^{4}$ | $10^{3} \mathrm{~mm}^{3}$ | mm | $10^{6} \mathrm{~mm}^{4}$ | $10^{3} \mathrm{~mm}^{3}$ | $10^{3} \mathrm{~mm}^{3}$ | mm |
| $64 \times 41 \times 1.55$ LC - G450 | 63.5 | 41.3 | 10.0 | 1.55 | 1.5 | 15.1 | 1.90 | 242 | 0.163 | 5.14 | 26.0 | 0.0556 | 2.12 | 3.68 | 15.2 |
| $64 \times 41 \times 1.15$ LC - G500 | 63.5 | 41.3 | 10.0 | 1.15 | 1.5 | 15.1 | 1.43 | 182 | 0.124 | 3.91 | 26.2 | 0.0428 | 1.64 | 2.83 | 15.4 |
| $64 \times 41 \times 0.95$ LC - G550 | 63.5 | 41.3 | 10.0 | 0.95 | 1.5 | 15.1 | 1.19 | 151 | 0.104 | 3.28 | 26.3 | 0.0360 | 1.38 | 2.38 | 15.4 |
| $64 \times 41 \times 0.75$ LC - G550 | 63.5 | 41.3 | 10.0 | 0.75 | 1.5 | 15.1 | 0.941 | 120 | 0.0832 | 2.62 | 26.3 | 0.0290 | 1.11 | 1.91 | 15.5 |

## NOTES:

1. Calculations of section properties are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).


Table 1.2

## SECTION PROPERTIES TO CALCULATE MEMBER STABILITY



| DIMENSIONS |  |  |  |  |  |  |  |  | RATIOS |  | PROPERTIES |  |  |  |  | MATERIAL |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Designation | Depth <br> d | Flange Width <br> $b_{\mathrm{f}}$ | Lip Depth $d_{\mathrm{L}}$ | Thickness <br> $t$ | Inside <br> Corner <br> Radius <br> $r_{i}$ | Flat <br> Web <br> Depth <br> $d_{1}$ | Flat Flange Width b | Mass per metre | Web $d_{1} / t$ | Flange <br> b/t | Shear <br> Centre Co-ord. <br> $x_{0}$ | Polar Rad. of Gyration about S.C. $r_{01}$ | MonoSymmetry Constant $\beta_{y}$ | Torsion Constant <br> $J$ | Warping Constant $I_{\mathrm{w}}$ | Grade | Design <br> Yield <br> Stress <br> $f_{y}$ | Design <br> Tensile <br> Strength <br> $f_{u}$ |
|  | mm | mm | mm | mm | mm | mm | mm | kg/m |  |  | mm | mm |  | mm ${ }^{4}$ | $10^{6} \mathrm{~mm}^{6}$ |  | MPa | MPa |
| $64 \times 41 \times 1.55$ LC - G450 | 63.5 | 41.3 | 10.0 | 1.55 | 1.5 | 57.4 | 35.2 | 1.90 | 37.0 | 22.7 | 34.6 | 45.9 | 89.1 | 194 | 51.1 | G450 | 450 | 480 |
| $64 \times 41 \times 1.15$ LC - G500 | 63.5 | 41.3 | 10.0 | 1.15 | 1.5 | 58.2 | 36.0 | 1.43 | 50.6 | 31.3 | 35.1 | 46.4 | 90.0 | 80.1 | 39.9 | G500 | 500 | 520 |
| $64 \times 41 \times 0.95$ LC - G550 | 63.5 | 41.3 | 10.0 | 0.95 | 1.5 | 58.6 | 36.4 | 1.19 | 61.7 | 38.3 | 35.3 | 46.6 | 90.4 | 45.4 | 33.8 | G550 | 550 | 550 |
| $64 \times 41 \times 0.75$ LC - G550 | 63.5 | 41.3 | 10.0 | 0.75 | 1.5 | 59.0 | 36.8 | 0.941 | 78.7 | 49.1 | 35.6 | 46.9 | 90.9 | 22.5 | 27.4 | G550 | 495 | 495 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. The flat flange width is the average of the flanges.

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Table 2.1

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

## bending about $\mathbf{x}$-axis

$C_{b}=1.0$


| Designation | Mass per metre | Buckling Capacities |  | Design Member Moment Capacity, $\phi_{\mathrm{b}} M_{\mathrm{bx}}(\mathrm{kNm})$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Local $\phi_{b} M_{\mathrm{sx}}$ | Distortional $\phi_{\mathrm{b}} M_{\mathrm{bdx}}$ | Effective Length $\left(L_{\mathrm{e}}\right)$ in metres |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | kg/m | kNm | kNm | 0.2 | 0.3 | 0.6 | 0.9 | 1.2 | 1.5 | 1.8 | 2.1 | 2.4 | 2.7 | 3 | 3.3 | 3.6 | 4 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 2.08 | 1.92 | 2.01 | 1.92 | 1.92 | 1.92 | 1.73 | 1.45 | 1.13 | 0.879 | 0.714 | 0.598 | 0.514 | 0.450 | 0.400 | 0.348 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 1.71 | 1.39 | 1.64 | 1.39 | 1.39 | 1.39 | 1.39 | 1.10 | 0.806 | 0.614 | 0.489 | 0.402 | 0.340 | 0.293 | 0.257 | 0.220 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 1.34 | 1.14 | 1.34 | 1.15 | 1.14 | 1.14 | 1.12 | 0.918 | 0.656 | 0.495 | 0.390 | 0.318 | 0.266 | 0.227 | 0.198 | 0.168 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.853 | 0.775 | 0.853 | 0.814 | 0.775 | 0.775 | 0.730 | 0.619 | 0.492 | 0.384 | 0.300 | 0.242 | 0.200 | 0.170 | 0.146 | 0.122 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. Capacities are calculated for a uniform bending moment ( $C_{b}=1.0$ ).
6. Refer to Graph 2.1 for the limits of the local and distortional design moment capacities.
7. The effective length $L_{e}=L_{e y}=L_{e z}$.


## Graph 2.1

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

## bending about x -axis

$C_{b}=1.0$



NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600
2. Thickness refers to the base metal thickness (BMT)
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. Capacities are calculated for a uniform bending moment ( $C_{b}=1.0$ )
6. The effective length $L_{e}=L_{e y}=L_{e z}$.


Table 2.2

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint
bending about $y$-axis
(Lips in Compression)
Compression


Tension
(Lips in Compression)

| Designation | Mass per metre | Buckling Capacities |  | Design Member Moment Capacity, $\phi_{\mathrm{b}} M_{\text {byL }}(\mathrm{kNm})$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Local $\phi_{\mathrm{b}} M_{\mathrm{syL}}$ | Distortional $\phi_{\mathrm{b}} M_{\text {bdyl }}$ | Effective Length $\left(L_{e}\right)$ in metres |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | kg/m | kNm | kNm | 0.2 | 0.3 | 0.6 | 0.9 | 1.2 | 1.5 | 1.8 | 2.1 | 2.4 | 2.7 | 3 | 3.3 | 3.6 | 4 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.860 | 0.808 | 0.860 | 0.808 | 0.808 | 0.787 | 0.679 | 0.562 | 0.446 | 0.365 | 0.312 | 0.275 | 0.248 | 0.228 | 0.212 | 0.196 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.736 | 0.593 | 0.736 | 0.597 | 0.593 | 0.593 | 0.533 | 0.396 | 0.293 | 0.231 | 0.190 | 0.162 | 0.142 | 0.127 | 0.116 | 0.104 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.681 | 0.488 | 0.668 | 0.500 | 0.488 | 0.488 | 0.457 | 0.318 | 0.231 | 0.178 | 0.144 | 0.121 | 0.104 | 0.0917 | 0.0822 | 0.0726 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.490 | 0.332 | 0.490 | 0.360 | 0.332 | 0.332 | 0.332 | 0.246 | 0.176 | 0.133 | 0.106 | 0.0872 | 0.0737 | 0.0637 | 0.0561 | 0.0485 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. Capacities are calculated for $C_{s}=1.0$ and for a uniform bending moment ( $C_{T F}=1.0$ ).
6. Refer to Graph 2.2 for the limits of the local and distortional design moment capacities.
7. The effective length $L_{e}=L_{e x}=L_{e z}$.


## Graph 2.2

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

## Compression



## bending about $\mathbf{y}$-axis

Tension
(Lips in Compression)


NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600
2. Thickness refers to the base metal thickness (BMT)
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. Capacities are calculated for $C_{s}=1.0$ and for a uniform bending moment ( $C_{T F}=1.0$ ).
6. The effective length $L_{e}=L_{e x}=L_{e z}$.


Table 2.3

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

## bending about $y$-axis <br> (Web in Compresion)



| Designation | Mass per metre | Buckling Capacities |  | Design Member Moment Capacity, $\phi_{\mathrm{b}} M_{\text {byw }}$ (kNm) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Local } \\ & \phi_{b} M_{\text {syw }} \end{aligned}$ | Distortional $\phi_{\mathrm{b}} M_{\mathrm{bdyw}}$ | Effective Length $\left(L_{e}\right)$ in metres |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | kg/m | kNm | kNm | 0.2 | 0.3 | 0.6 | 0.9 | 1.2 | 1.5 | 1.8 | 2.1 | 2.4 | 2.7 | 3 | 3.3 | 3.6 | 4 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.860 | N.A. | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 | 0.860 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.673 | N.A. | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 | 0.673 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.529 | N.A. | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 | 0.529 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.337 | N.A. | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 | 0.337 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. Capacities are calculated for $C_{s}=1.0$ and for a uniform bending moment $\left(C_{T F}=1.0\right)$.
6. Refer to Graph 2.3 for the limits of the local and distortional design moment capacities.
7. The effective lengths $L_{e}=L_{e x}=L_{e z}$.


Graph 2.3

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

## bending about $y$-axis <br> (Web in Compression)



NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600
2. Thickness refers to the base metal thickness (BMT)
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. Capacities are calculated for $C_{s}=1.0$ and for a uniform bending moment ( $C_{T F}=1.0$ ).
6. The effective length $L_{e}=L_{e x}=L_{e z}$.


Table 2.4

## SHEAR CAPACITIES

| Designation | Mass <br> per <br> metre | Shear Capacity <br> x -axis <br> $\phi_{v} V_{\mathrm{vx}}$ |  |  | y -axis <br> $\phi_{v} V_{\mathrm{vy}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | kN | kN |  |  |  |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 23.1 | 28.3 |  |  |
| $64 \times 41 \times 1.15$ LC -G 500 | 1.43 | 17.6 | 23.8 |  |  |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 12.6 | 21.9 |  |  |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 6.22 | 14.9 |  |  |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600 .
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.


## Graph 2.4

## COMBINED BENDING \& SHEAR

## bending about $x$-axis




1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.


## Graph 2.5

## COMBINED BENDING \& SHEAR

## bending about y-axis

(Lips in Compression)

## Compression



Tension

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.


## Graph 2.6

## COMBINED BENDING \& SHEAR

## bending about y-axis <br> (Web in Compression)




## NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.


Table 2.5

## WEB BEARING CAPACITY

One Flange Loading or Reaction


| Designation | Mass per metre | $1.5 \mathrm{~d}_{1}$ | Design Web Bearing Capacity, $\phi_{\mathrm{w}} R_{\mathrm{bx}}(\mathrm{kN})$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | End Bearing ( $\mathrm{c}<1.5 \mathrm{~d}_{1}$ ) |  |  |  |  |  | Interior Bearing ( $c \geq 1.5 \mathrm{~d}_{1}$ ) |  |  |  |  |  |
|  |  |  | Bearing Length, $L_{\mathrm{b}}(\mathrm{mm})$ |  |  |  |  |  | Bearing Length, $L_{\mathrm{b}}(\mathrm{mm})$ |  |  |  |  |  |
|  | kg/m | mm | 25 | 50 | 75 | 100 | 125 | 150 | 25 | 50 | 75 | 100 | 125 | 150 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 86.1 | 6.30 | 7.83 | 9.00 | 10.0 | 10.9 | 11.6 | 14.4 | 16.5 | 18.1 | 19.5 | 20.7 | 21.9 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 87.3 | 4.01 | 5.04 | 5.83 | 6.50 | 7.09 | 7.62 | 8.76 | 10.2 | 11.3 | 12.2 | 13.0 | 13.8 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 87.9 | 3.08 | 3.90 | 4.53 | 5.07 | 5.53 | 5.96 | 6.54 | 7.67 | 8.54 | 9.27 | 9.92 | 10.5 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 88.5 | 1.78 | 2.27 | 2.65 | 2.96 | 3.24 | 3.50 | 3.62 | 4.29 | 4.81 | 5.24 | 5.62 | 5.97 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.


Table 2.6

## WEB BEARING CAPACITY

Two Flange Loading or Reaction


End Bearing ( $c<1.5 d_{1}$ )
Interior Bearing ( $c \geq 1.5 d_{1}$ )

| Designation | Mass per metre | $1.5 \mathrm{~d}_{1}$ | Design Web Bearing Capacity, $\phi_{\mathrm{w}} R_{\mathrm{bx}}(\mathrm{kN})$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | End Bearing ( $c<1.5 \mathrm{~d}_{1}$ ) |  |  |  |  |  | Interior Bearing ( $c \geq 1.5 \mathrm{~d}_{1}$ ) |  |  |  |  |  |
|  |  |  | Bearing Length, $L_{\mathrm{b}}(\mathrm{mm})$ |  |  |  |  |  | Bearing Length, $L_{\mathrm{b}}(\mathrm{mm})$ |  |  |  |  |  |
|  | kg/m | mm | 25 | 50 | 75 | 100 | 125 | 150 | 25 | 50 | 75 | 100 | 125 | 150 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 86.1 | 7.87 | 8.42 | 8.84 | 9.19 | 9.50 | 9.78 | 16.1 | 18.7 | 20.6 | 22.2 | 23.7 | 24.9 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 87.3 | 4.33 | 4.67 | 4.93 | 5.15 | 5.34 | 5.52 | 8.70 | 10.2 | 11.3 | 12.3 | 13.1 | 13.9 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 87.9 | 2.99 | 3.25 | 3.44 | 3.60 | 3.75 | 3.88 | 5.80 | 6.84 | 7.64 | 8.32 | 8.92 | 9.45 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 88.5 | 1.48 | 1.62 | 1.73 | 1.82 | 1.89 | 1.96 | 2.62 | 3.12 | 3.51 | 3.83 | 4.12 | 4.38 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.


Graph 2.7
COMBINED BENDING \& BEARING
bending about $x$-axis


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Graph 2.8
COMBINED BENDING \& BEARING
bending about $x$-axis




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Graph 2.9

## COMBINED BENDING \& BEARING

bending about $x$-axis




## CONTENTS

Part 3: Members subject to Axial Compression
Table 3.1: Axial Compression Capacity
Graph 3.1: Axial Compression Capacity

## Part 3: <br> Members subject to Axial Compression



Table 3.1

## AXIAL COMPRESSION CAPACITY

$L_{\mathrm{ex}}=L_{\mathrm{ey}}=L_{\mathrm{ez}}$


| Designation | Mass per metre | Buckling Capacities |  | Design Axial Compression Capacities, $\phi_{\mathrm{c}} N_{\mathrm{c}}(\mathrm{kN})$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Local <br> $\phi_{c} N_{s}$ | Distortional $\phi_{\mathrm{c}} N_{\mathrm{cd}}$ | Effective Length $\left(L_{\mathrm{e}}\right)$ in metres |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | kg/m | kN | kN | 0.2 | 0.3 | 0.6 | 0.9 | 1.2 | 1.5 | 1.8 | 2.1 | 2.4 | 2.7 | 3 | 3.3 | 3.6 | 4 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 86.5 | 72.3 | 80.0 | 80.0 | 64.8 | 43.5 | 27.3 | 19.0 | 14.5 | 11.7 | 9.92 | 8.64 | 7.68 | 6.95 | 6.31 | 5.11 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 57.0 | 49.7 | 55.4 | 53.3 | 43.8 | 31.9 | 19.2 | 12.9 | 9.53 | 7.47 | 6.12 | 5.19 | 4.51 | 4.01 | 3.61 | 3.21 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 44.1 | 39.3 | 42.7 | 41.0 | 33.2 | 23.4 | 15.6 | 10.3 | 7.50 | 5.77 | 4.65 | 3.88 | 3.32 | 2.91 | 2.59 | 2.27 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 27.6 | 26.0 | 26.8 | 25.9 | 21.4 | 15.7 | 10.9 | 7.97 | 5.69 | 4.31 | 3.42 | 2.80 | 2.36 | 2.03 | 1.78 | 1.53 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. Refer to Graph 3.1 for the limits of the local and distortional design moment capacities.
6. The effective length $L_{e}=L_{e x}=L_{e y}=L_{e z}$


## Graph 3.1

## AXIAL COMPRESSION CAPACITY

$$
L_{\mathrm{ex}}=L_{\mathrm{ey}}=L_{\mathrm{ez}}
$$




NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT)
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. The effective length $L_{e}=L_{e x}=L_{e y}=L_{e z}$.

## CONTENTS

Part 4: Members subject to Axial Tension Table 4.1: Axial Tension Capacity

## Part 4: <br> Members subject to Axial Tension



Table 4.1

## AXIAL TENSION CAPACITIES

with and without holes


| Designation | Mass per metre | Design Axial Tension Capacity, $\phi_{\mathrm{t}} N_{\mathrm{t}}(\mathrm{kN})$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Uniform Tension | Web Connected |  |  |  |  |  |  | Both Flanges Connected |  |  |  |  |  |  |
|  |  |  | Total hole Width, $\mathrm{w}_{\mathrm{h}}$ (m) |  |  |  |  |  |  | Total hole Width, $w_{\text {h }}(\mathrm{m})$ |  |  |  |  |  |  |
|  | kg/m | (NO Holes) | 0 | 10 | 20 | 25 | 30 | 35 | 40 | 0 | 10 | 20 | 25 | 30 | 35 | 40 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 97.9 | 75.5 | 70.6 | 65.8 | 63.4 | 61.0 | 58.5 | 56.1 | 75.5 | 70.6 | 65.8 | 63.4 | 61.0 | 58.5 | 56.1 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 81.7 | 61.4 | 57.5 | 53.6 | 51.7 | 49.7 | 47.8 | 45.9 | 61.4 | 57.5 | 53.6 | 51.7 | 49.7 | 47.8 | 45.9 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 74.7 | 54.0 | 50.6 | 47.2 | 45.5 | 43.8 | 42.1 | 40.4 | 54.0 | 50.6 | 47.2 | 45.5 | 43.8 | 42.1 | 40.4 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 53.4 | 38.6 | 36.2 | 33.8 | 32.6 | 31.4 | 30.1 | 28.9 | 38.6 | 36.2 | 33.8 | 32.6 | 31.4 | 30.1 | 28.9 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

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Part 5: Members subject to Combined Actions
Table 5.1: $\quad$ Section \& Yield Capacities
Table 5.2: Elastic Buckling Load (x-axis)
Table 5.3: $\quad$ Elastic Buckling Load (y-axis)

## Part 5: <br> Members subject to Combined Actions

DESIGN CAPACITY TABLES for $64 \times 41$ Lipped Channels to AS/NZS 4600


Table 5.1
SECTION \& YIELD CAPACITIES

| Designation | Mass <br> per m | Design Section Axial Capacities |  | Design Section Moment Capacities |  |  | Design Yield Moment Capacities (Tension) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Tension | Compression | $\begin{gathered} \text { about } x \text {-axis } \\ \phi_{b} M_{s x} \end{gathered}$ | about y-axis |  | about $x$-axis$\phi_{b} M_{\mathrm{sxf}}$ | about y -axis |  |
|  |  | $\phi_{\mathrm{t}} N_{\mathrm{t}}$ | $\phi_{C} N_{s}$ |  | $\phi_{b} M_{\text {syL }}$ | $\phi_{b} M_{\text {syW }}$ |  | $\phi_{b} M_{\text {syfL }}$ | $\phi_{\mathrm{b}} M_{\text {syfW }}$ |
|  | $\mathrm{kg} / \mathrm{m}$ | kN | kN | kNm | kNm | kNm | kNm | kNm | kNm |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 97.9 | 86.5 | 2.08 | 0.860 | 0.860 | 2.08 | 0.860 | 1.49 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 81.7 | 57.0 | 1.71 | 0.736 | 0.673 | 1.76 | 0.736 | 1.27 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 74.7 | 44.1 | 1.34 | 0.681 | 0.529 | 1.62 | 0.681 | 1.18 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 53.4 | 27.6 | 0.853 | 0.490 | 0.337 | 1.17 | 0.493 | 0.852 |

## NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. $\phi_{\mathrm{b}} M_{\text {syL }}$ and $\phi_{\mathrm{b}} M_{\text {syw }}$ refer to bending about the $y$-axis causing compression in the lips and web of the channel respectively.
6. $\phi_{b} M_{\text {syfL }}$ and $\phi_{b} M_{\text {syfw }}$ are the design yield moments for bending about the $y$-axis causing tension in the lips and web of the channel respectively.
7. Capacities are calculated for an equal flange lipped channel using the average flange width.


Table 5.2

## ELASTIC BUCKLING LOAD

buckling about $x$-axis


| Designation | Mass per metre | Elastic Buckling Load, $N_{\text {ex }}(\mathrm{kN})$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Effective Length, $L_{\text {ex }}(\mathrm{m})$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | kg/m | 0.6 | 1.2 | 1.5 | 1.8 | 2.1 | 2.4 | 2.7 | 3 | 3.3 | 3.6 | 4 | 4.5 | 5 | 6 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 895 | 224 | 143 | 99.4 | 73.0 | 55.9 | 44.2 | 35.8 | 29.6 | 24.9 | 20.1 | 15.9 | 12.9 | 8.95 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 681 | 170 | 109 | 75.7 | 55.6 | 42.6 | 33.7 | 27.3 | 22.5 | 18.9 | 15.3 | 12.1 | 9.81 | 6.81 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 570 | 143 | 91.3 | 63.4 | 46.6 | 35.6 | 28.2 | 22.8 | 18.9 | 15.8 | 12.8 | 10.1 | 8.21 | 5.70 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 456 | 114 | 73.0 | 50.7 | 37.2 | 28.5 | 22.5 | 18.2 | 15.1 | 12.7 | 10.3 | 8.11 | 6.57 | 4.56 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.


Table 5.3

## ELASTIC BUCKLING LOAD

buckling about $y$-axis


| Designation | Mass per metre | Elastic Buckling Load, $N_{\text {ey }}(\mathrm{kN})$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Effective Length, $L_{\text {ey }}(\mathrm{m})$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | kg/m | 0.6 | 1.2 | 1.5 | 1.8 | 2.1 | 2.4 | 2.7 | 3.0 | 3.3 | 3.6 | 4.0 | 4.5 | 5.0 | 6.0 |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 305 | 76.2 | 48.8 | 33.9 | 24.9 | 19.1 | 15.1 | 12.2 | 10.1 | 8.47 | 6.86 | 5.42 | 4.39 | 3.05 |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 235 | 58.7 | 37.6 | 26.1 | 19.2 | 14.7 | 11.6 | 9.39 | 7.76 | 6.52 | 5.28 | 4.17 | 3.38 | 2.35 |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 197 | 49.4 | 31.6 | 21.9 | 16.1 | 12.3 | 9.75 | 7.90 | 6.53 | 5.49 | 4.44 | 3.51 | 2.84 | 1.97 |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 159 | 39.7 | 25.4 | 17.6 | 13.0 | 9.92 | 7.84 | 6.35 | 5.25 | 4.41 | 3.57 | 2.82 | 2.29 | 1.59 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

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Graph 6.1: Combined Bending \& Shear (bending about y-axis)

## GENERAL

When these lipped channel sections are used in frames and trusses, there will be instances where the lips of the sections are removed at the location of the connections. This part of the document provides design tables and graphs which will aid in the design of the unlipoped sections produced by removing the lips. The diagram below illustrates the portion of the section which is removed.

DESIGN CAPACITY TABLES for 64 x 41 Lipped Channels to AS/NZS 4600
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Table 6.1


## DIMENSIONS \& SECTION PROPERTIES

Lips Removed


| DIMENSIONS |  |  |  |  |  |  | SECTION PROPERTIES |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Designation | Depth <br> d | Flange Width $b_{\text {f }}$ | Thickness <br> $t$ | Inside <br> Corner <br> Radius <br> $r_{i}$ | Co-ord. <br> of <br> Centroid $x_{c}$ | Mass per metre | Gross <br> Section <br> Area <br> $A_{g}$ | $I_{x}$ | About x-axi $Z_{x}$ | $r_{\text {x }}$ | $I_{y}$ | $Z_{y L}$ | axis $Z_{y w}$ | $r_{y}$ |
|  | mm | mm | mm | mm | mm | kg/m | $\mathrm{mm}^{2}$ | $10^{6} \mathrm{~mm}^{4}$ | $10^{3} \mathrm{~mm}^{3}$ | mm | $10^{6} \mathrm{~mm}^{4}$ | $10^{3} \mathrm{~mm}^{3}$ | $10^{3} \mathrm{~mm}^{3}$ | mm |
| $64 \times 41 \times 1.55$ LC-LR - G450 | 63.5 | 38.3 | 1.55 | 1.5 | 11.2 | 1.64 | 209 | 0.139 | 4.39 | 25.8 | 0.0317 | 1.17 | 2.84 | 12.3 |
| $64 \times 41 \times 1.15$ LC-LR - G500 | 63.5 | 38.7 | 1.15 | 1.5 | 11.2 | 1.23 | 157 | 0.106 | 3.35 | 26.0 | 0.0246 | 0.897 | 2.20 | 12.5 |
| $64 \times 41 \times 0.95$ LC-LR - G550 | 63.5 | 38.9 | 0.95 | 1.5 | 11.2 | 1.03 | 131 | 0.0891 | 2.81 | 26.1 | 0.0208 | 0.752 | 1.86 | 12.6 |
| $64 \times 41 \times 0.75$ LC-LR - G550 | 63.5 | 39.1 | 0.75 | 1.5 | 11.2 | 0.815 | 104 | 0.0713 | 2.25 | 26.2 | 0.0168 | 0.603 | 1.50 | 12.7 |

NOTES:

1. Calculations of section properties are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).

Table 6.2


## SECTION PROPERTIES TO CALCULATE MEMBER STABILITY




NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

Table 6.3


## SECTION \& YIELD CAPACITIES

Lips Removed



| Designation | Mass <br> per m | Design Section Axial Capacities |  | Design Section Moment Capacities |  |  | Design Yield Moment Capacities (Tension) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Tension | Compression | about $x$-axis$\phi_{b} M_{s x}$ | about y -axis |  | about $x$-axis$\phi_{\mathrm{b}} M_{\mathrm{sxf}}$ | about y -axis |  |
|  |  | $\phi_{t} N_{t}$ | $\phi_{\mathrm{C}} N_{\mathrm{s}}$ |  | $\phi_{b} M_{\text {syT }}$ | $\phi_{\mathrm{b}} M_{\text {syW }}$ |  | $\phi_{b} M_{\text {syfT }}$ | $\phi_{b} M_{\text {syfW }}$ |
|  | $\mathrm{kg} / \mathrm{m}$ | kN | kN | kNm | kNm | kNm | kNm | kNm | kNm |
| $64 \times 41 \times 1.55$ LC-LR - G450 | 1.64 | 84.7 | 55.8 | 1.32 | 0.397 | 0.475 | 1.78 | 0.475 | 1.15 |
| $64 \times 41 \times 1.15$ LC-LR - G500 | 1.23 | 70.8 | 36.0 | 0.867 | 0.263 | 0.404 | 1.51 | 0.404 | 0.992 |
| $64 \times 41 \times 0.95$ LC-LR - G550 | 1.03 | 64.7 | 27.5 | 0.668 | 0.204 | 0.328 | 1.39 | 0.372 | 0.922 |
| $64 \times 41 \times 0.75$ LC-LR - G550 | 0.815 | 46.3 | 17.1 | 0.417 | 0.128 | 0.209 | 1.00 | 0.269 | 0.670 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
5. $\phi_{b} M_{\text {syT }}$ and $\phi_{b} M_{\text {syw }}$ refer to bending about the y-axis causing compression in the toes and web of the channel respectively
6. $\phi_{b} M_{\text {syft }}$ and $\phi_{b} M_{\text {syfW }}$ are the design yield moment capacities for bending about the $y$-axis causing tension in the toes and web of the channel respectively.
7. All section moment capacities are applicable for unrestrained lengths up to 400 mm . Lips removed for more than this length is not expected.
8. Capacities are calculated for an equal flange channel using the average flange width.

Table 6.4


| Designation | Mass per metre <br> $\mathrm{kg} / \mathrm{m}$ | Design Axial Compression Capacity, $\phi_{c} N_{c}(\mathrm{kN})$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Effective Length $\left(L_{\mathrm{e}}\right)$ in metres |  |  |  |  |  |
|  |  | 0.0 | 0.10 | 0.20 | 0.30 | 0.35 | 0.40 |
| $64 \times 41 \times 1.55$ LC-LR - G450 | 1.64 | 55.8 | 55.3 | 53.8 | 51.5 | 50.1 | 48.5 |
| $64 \times 41 \times 1.15$ LC-LR - G500 | 1.23 | 36.0 | 35.7 | 34.6 | 33.0 | 32.0 | 30.9 |
| $64 \times 41 \times 0.95$ LC-LR - G550 | 1.03 | 27.5 | 27.2 | 26.4 | 25.1 | 24.2 | 23.3 |
| $64 \times 41 \times 0.75$ LC-LR - G550 | 0.815 | 17.1 | 16.9 | 16.5 | 15.7 | 15.3 | 14.7 |

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.
2. Thickness refers to the base metal thickness (BMT).
3. Steel grades are in accordance with AS 1397.
4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600.
5. Refer to Graph 3.1 for the limits of the local and distortional design moment capacities.
6. The effective length $L_{e}=L_{e x}=L_{e y}=L_{e z}$.


Graph 6.1


Toes in Compression

## COMBINED BENDING \& SHEAR

## bending about $y$-axis

Lips Removed


Web in Compression



## CONTENTS

## Part 7: Wall Framing Design Capacities

Table 7.1: $\quad$ Wall stud Design Capacities - Unclad
Table 7.1: Wall stud Design Capacities - Clad Both Sides
Table 7.2: $\quad$ Wall Plate Design Capacities

## Part 7: Wall Framing Design Capacities

## GENERAL

This part of the Design Capacity tables provide capacities which may be used for the design of the sections as wall studs and wall plates. Three typical wall heights are specified for the wall studs.

The NASH wall stud and plate classifications for both Australia and New Zealand are also included in the tables for each section. These are based on the minimum properties and capacities given in the NASH references.

DESIGN CAPACITY TABLES for 64 x 41 Lipped Channels to AS/NZS 4600
Version 01 - June 2019 - Page 6-7

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## Table 7.1



## WALL STUD

 DESIGN CAPACITIESUnclad


| Designation | Mass per metre <br> $\mathrm{kg} / \mathrm{m}$ | Design Properties and Capacities |  |  |  |  |  |  |  |  | NASH <br> Wall Stud Classification |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Lateral Actions |  |  |  | Co <br> $\phi_{c} N_{s}$ | Compression | Tension $\phi_{\mathrm{t}} N_{\mathrm{t}}$ | Comb <br> $\phi_{b} M_{\text {sxf }}$ | cions $N_{\text {ex }}$ |  |  |
|  |  | $10^{6} \mathrm{~mm}^{4}$ | kNm | kNm | kN | kN | kN | kN | kNm | kN | Australia | New Zealand |
| Stud Height 2440 mm |  |  |  |  |  |  |  |  |  |  |  |  |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.163 | 2.08 | 1.92 | 23.1 | 86.5 | 29.0 | 75.5 | 2.08 | 84.5 | SC | SD |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.124 | 1.71 | 1.39 | 17.6 | 57.0 | 21.2 | 61.4 | 1.76 | 64.4 | SC | SD |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.104 | 1.34 | 1.14 | 12.6 | 44.1 | 17.4 | 54.0 | 1.62 | 53.9 | SC | SC |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.0832 | 0.853 | 0.775 | 6.22 | 27.6 | 11.8 | 38.6 | 1.17 | 43.1 | SA | SB |
| Stud Height 2740 mm |  |  |  |  |  |  |  |  |  |  |  |  |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.163 | 2.08 | 1.82 | 23.1 | 86.5 | 23.4 | 75.5 | 2.08 | 67.0 | SC | SD |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.124 | 1.71 | 1.39 | 17.6 | 57.0 | 17.0 | 61.4 | 1.76 | 51.1 | SC | SB |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.104 | 1.34 | 1.14 | 12.6 | 44.1 | 14.0 | 54.0 | 1.62 | 42.7 | SB | SB |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.0832 | 0.853 | 0.762 | 6.22 | 27.6 | 10.2 | 38.6 | 1.17 | 34.2 | SA | SB |
| Stud Height 3040 mm |  |  |  |  |  |  |  |  |  |  |  |  |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.163 | 2.08 | 1.92 | 23.1 | 86.5 | 27.4 | 75.5 | 2.08 | 54.5 | SC | SD |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.124 | 1.71 | 1.39 | 17.6 | 57.0 | 20.5 | 61.4 | 1.76 | 41.5 | SC | SD |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.104 | 1.34 | 1.14 | 12.6 | 44.1 | 17.1 | 54.0 | 1.62 | 34.7 | SC | SC |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.0832 | 0.853 | 0.775 | 6.22 | 27.6 | 11.7 | 38.6 | 1.17 | 27.8 | SA | SC |

## Wall Stud Design Assumptions

| Effective Lengths for Design |  |  |  |
| :---: | :---: | :---: | :---: |
| Stud Height $(\mathrm{mm})$ | 2440 | 2740 | 3040 |
| No. of Noggings | 1 | 1 | 2 |
| $L_{\mathrm{ex}}(\mathrm{mm})$ | 1952 | 2192 | 2432 |
| $L_{\mathrm{ey}}(\mathrm{mm})$ | 976 | 1096 | 810 |
| $L_{\mathrm{ez}}(\mathrm{mm})$ | 976 | 1096 | 810 |

## NOTES:

1. Noggings are equally spaced.
2. Lateral restraint is assumed to be provided by noggings only. Additional lateral restraint provided by cladding is ignored.
3. Both flanges of the stud are restrained by the top and bottom plates and the noggings.
4. Effective lengths are taken as $80 \%$ of the distance between restraints in accordance with NASH Handbook Clause 3.4.2.
5. No allowance has been made for holes in the web of the stud.

| Symbol | Description |
| :---: | :--- |
| $I_{\mathrm{x}}$ | second moment of area about the major principal x-axis |
| $\phi_{\mathrm{c}} N_{\mathrm{s}}$ | design section capacity of a member in compression |
| $\phi_{\mathrm{c}} N_{\mathrm{c}}$ | design member capacity of a member in compression |
| $\phi_{\mathrm{b}} M_{\mathrm{sx}}$ | design section moment capacity about the x-axis |
| $\phi_{\mathrm{b}} M_{\mathrm{bx}}$ | design member moment capacity about the x-axis |
| $\phi_{\mathrm{b}} M_{\mathrm{sxf}}$ | design yield moment capacity about the x-axis |
| $\phi_{\mathrm{v}} V_{\mathrm{vx}}$ | design shear capacity of the cross-section perpendicular to the x-axis |
| $N_{\mathrm{ex}}$ | elastic buckling load about the major principal x-axis |
| $\phi_{\mathrm{t}} N_{\mathrm{t}}$ | design section capacity of a member in tension |
| $L_{\mathrm{ex}}$ | effective length for buckling about the major principal x-axis |
| $L_{\mathrm{ey}}$ | effective length for buckling about the minor principal y-axis |
| $L_{\mathrm{ez}}$ | effective length for torsional buckling about the longitudinal z-axis |

## References

AS/NZS 4600 Cold-Formed Steel Structures.
NASH Standard (NZ), Residential and Low-Rise Steel Framing, Part 1: Design Criteria. NASH Standard (Aust.), Residential and Low-Rise Steel Framing, Part 2: Design Solutions.
NASH Handbook (Aust.), Best Practice for Design and Construction of Residential and LowRise Steel Framing, Chapter 3.

Table 7.2


## WALL STUD

 DESIGN CAPACITIESClad Both Sides



| Designation | Mass per metre <br> $\mathrm{kg} / \mathrm{m}$ | Design Properties and Capacities |  |  |  |  |  |  |  |  | NASH <br> Wall Stud Classification |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Lateral Actions |  |  |  | Compression |  | Tension $\phi_{\mathrm{t}} N_{\mathrm{t}}$ | Comb <br> $\phi_{b} M_{\text {sxf }}$ | cions $N_{\text {ex }}$ |  |  |
|  |  | $10^{6} \mathrm{~mm}^{4}$ | kNm | kNm | kN | kN | kN | kN | kNm | kN | Australia | New Zealand |
| Stud Height 2440 mm |  |  |  |  |  |  |  |  |  |  |  |  |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.163 | 2.08 | 1.92 | 23.1 | 86.5 | 43.0 | 75.5 | 2.08 | 84.5 | SC | SD |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.124 | 1.71 | 1.39 | 17.6 | 57.0 | 32.3 | 61.4 | 1.76 | 64.4 | SC | SD |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.104 | 1.34 | 1.14 | 12.6 | 44.1 | 24.0 | 54.0 | 1.62 | 53.9 | SC | SC |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.0832 | 0.853 | 0.775 | 6.22 | 27.6 | 16.1 | 38.6 | 1.17 | 43.1 | SA | SB |
| Stud Height 2740 mm |  |  |  |  |  |  |  |  |  |  |  |  |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.163 | 2.08 | 1.92 | 23.1 | 86.5 | 37.7 | 75.5 | 2.08 | 67.0 | SC | SD |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.124 | 1.71 | 1.39 | 17.6 | 57.0 | 28.6 | 61.4 | 1.76 | 51.1 | SC | SD |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.104 | 1.34 | 1.14 | 12.6 | 44.1 | 21.5 | 54.0 | 1.62 | 42.7 | SC | SC |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.0832 | 0.853 | 0.775 | 6.22 | 27.6 | 14.7 | 38.6 | 1.17 | 34.2 | SA | SB |
| Stud Height 3040 mm |  |  |  |  |  |  |  |  |  |  |  |  |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.163 | 2.08 | 1.92 | 23.1 | 86.5 | 32.4 | 75.5 | 2.08 | 54.5 | SC | SD |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.124 | 1.71 | 1.39 | 17.6 | 57.0 | 24.5 | 61.4 | 1.76 | 41.5 | SC | SD |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.104 | 1.34 | 1.14 | 12.6 | 44.1 | 19.4 | 54.0 | 1.62 | 34.7 | SC | SC |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.0832 | 0.853 | 0.775 | 6.22 | 27.6 | 13.2 | 38.6 | 1.17 | 27.8 | SA | SB |

## Wall Stud Design Assumptions

| Effective Lengths for Design |  |  |  |
| :---: | :---: | :---: | :---: |
| Stud Height $(\mathrm{mm})$ | 2440 | 2740 | 3040 |
| No. of Noggings | 1 | 1 | 2 |
| $L_{\mathrm{ex}}(\mathrm{mm})$ | 1952 | 2192 | 2432 |
| $L_{\mathrm{ey}}(\mathrm{mm})$ | 600 | 600 | 600 |
| $L_{\mathrm{ez}}(\mathrm{mm})$ | 600 | 600 | 600 |

## NOTES:

1. Noggings are equally spaced.
2. Lateral restraint is assumed to be provided the cladding.
3. Both flanges of the stud are restrained by the top and bottom plates, the nogging, and the cladding
4. Effective length $\mathrm{L}_{\mathrm{ex}}$ is taken as $80 \%$ of the ength of the stud in accordance with NASH Handbook Clause 3.4.2.
5. Effective lengths $L_{e y}$ and $L_{e z}$ are assumed to be as per the table above.
6. No allowance has been made for holes in the web of the stud.

| Symbol | Description |
| :---: | :--- |
| $I_{\mathrm{x}}$ | second moment of area about the major principal x-axis |
| $\phi_{\mathrm{c}} N_{\mathrm{s}}$ | design section capacity of a member in compression |
| $\phi_{\mathrm{c}} N_{\mathrm{c}}$ | design member capacity of a member in compression |
| $\phi_{\mathrm{b}} M_{\mathrm{sx}}$ | design section moment capacity about the x-axis |
| $\phi_{\mathrm{b}} M_{\mathrm{bx}}$ | design member moment capacity about the x-axis |
| $\phi_{\mathrm{b}} M_{\mathrm{sxf}}$ | design yield moment capacity about the x-axis |
| $\phi_{\mathrm{v}} V_{\mathrm{vx}}$ | design shear capacity of the cross-section perpendicular to the x-axis |
| $N_{\mathrm{ex}}$ | elastic buckling load about the major principal x-axis |
| $\phi_{\mathrm{t}} N_{\mathrm{t}}$ | design section capacity of a member in tension |
| $L_{\mathrm{ex}}$ | effective length for buckling about the major principal x-axis |
| $L_{\mathrm{ey}}$ | effective length for buckling about the minor principal y-axis |
| $L_{\mathrm{ez}}$ | effective length for torsional buckling about the longitudinal z-axis |

## References

AS/NZS 4600 Cold-Formed Steel Structures.
NASH Standard (NZ), Residential and Low-Rise Steel Framing, Part 1: Design Criteria. NASH Standard (Aust.), Residential and Low-Rise Steel Framing, Part 2: Design Solutions.
NASH Handbook (Aust.), Best Practice for Design and Construction of Residential and LowRise Steel Framing, Chapter 3.

Table 7.3


## WALL PLATE DESIGN CAPACITIES



| Designation | Mass per metre | Design Properties and Capacities |  |  |  |  |  |  |  | NASH <br> Wall Plate Classification |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Full Lipped Channel (at midspan) |  |  |  | Channel Lips Removed (at supports) |  |  |  |  |  |
|  |  | $I_{y}$ | $\phi_{\mathrm{c}} N_{\mathrm{c}}$ | $\phi_{\mathrm{b}} M_{\text {byL }}$ | $\phi_{\mathrm{b}} M_{\text {byw }}$ | $\phi_{C} N_{s}$ | $\phi_{b} M_{\text {sy }}$ | $\phi_{\mathrm{b}} M_{\text {syw }}$ | $\phi_{v} V_{v y}$ |  |  |
|  | kg/m | $10^{6} \mathrm{~mm}^{4}$ | kN | kNm | kNm | kN | kNm | kNm | kN | Australia | New Zealand |
| $64 \times 41 \times 1.55$ LC - G450 | 1.90 | 0.0556 | 64.8 | 0.808 | 0.860 | 55.8 | 0.397 | 0.475 | 28.3 | PC | PE |
| $64 \times 41 \times 1.15$ LC - G500 | 1.43 | 0.0428 | 43.8 | 0.593 | 0.673 | 36.0 | 0.263 | 0.404 | 23.8 | PC | PD |
| $64 \times 41 \times 0.95$ LC - G550 | 1.19 | 0.0360 | 33.2 | 0.488 | 0.529 | 27.5 | 0.204 | 0.328 | 21.9 | PB | PC |
| $64 \times 41 \times 0.75$ LC - G550 | 0.941 | 0.0290 | 21.4 | 0.332 | 0.337 | 17.1 | 0.128 | 0.209 | 14.9 | PA | PB |

## NOTES:

1. The capacities for the full lipped channels are based on an effective length $L_{e}=0.6 \mathrm{~m}$.
2. The capacities of channels with lips removed are section capacities.
3. No allowance has been made for holes in the web of the plate in the determination of $l_{y}$
4. The NASH Classifications are based on the capacities of the full lipped channels.
5. The second moment of area $I_{y}$ for the full lipped channel is used for the NASH Australia classification.

| Symbol | Description |
| :---: | :--- |
| $I_{\mathrm{y}}$ | second moment of area about the minor principal y-axis |
| $\phi_{\mathrm{c}} N_{\mathrm{s}}$ | design section capacity of a member in compression |
| $\phi_{\mathrm{c}} N_{\mathrm{c}}$ | design member capacity of a member in compression |
| $\phi_{\mathrm{b}} M_{\mathrm{byL}}$ | design section moment capacity about the y-axis (lips in compression) |
| $\phi_{\mathrm{b}} M_{\mathrm{byw}}$ | design member moment capacity about the y-axis (web in compression) |
| $\phi_{\mathrm{b}} M_{\text {syT }}$ | design section moment capacity about the y-axis (toes in compression) |
| $\phi_{\mathrm{b}} M_{\text {syw }}$ | design section moment capacity about the y-axis (web in compression |
| $\phi_{\mathrm{v}} V_{\mathrm{vy}}$ | design shear capacity of the cross-section perpendicular to the y-axis |
| $L_{\mathrm{e}}$ | effective length $\left(L_{\mathrm{ex}}=L_{\mathrm{ey}}=L_{\mathrm{ez}}\right)$ |

## CONTENTS

## Appendix A: SIGNATURE CURVES

## Appendix A: Signature Curves

General
Graph A.1: $100 \times 50 \times 1.55$ LC - Axial Compression
Graph A.2: $100 \times 50 \times 1.55$ LC - Bending about $x$-axis
Graph A.3: $\quad 100 \times 50 \times 1.55$ LC - Bending about $y$-axis (Lips in Compression)
Graph A.4: $100 \times 50 \times 1.55$ LC - Bending about y -axis (Web in Compression)
Graph A.5: $\quad 100 \times 50 \times 1.15$ LC - Axial Compression
Graph A.6: $100 \times 50 \times 1.15$ LC - Bending about $x$-axis
Graph A.7: $100 \times 50 \times 1.15$ LC - Bending about $y$-axis (Lips in Compression)
Graph A.8: $100 \times 50 \times 1.15$ LC - Bending about y-axis (Web in Compression)
Graph A.9: $100 \times 50 \times 0.95$ LC - Axial Compression
Graph A.10: $100 \times 50 \times 0.95$ LC - Bending about $x$-axis
Graph A.11: $100 \times 50 \times 0.95$ LC - Bending about $y$-axis (Lips in Compression)
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Graph A. 14: $100 \times 50 \times 0.75$ LC - Bending about $x$-axis
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Graph A.16: $100 \times 50 \times 0.75$ LC - Bending about $y$-axis (Web in Compression

## GENERAL

This appendix provides the signature curves for each of the sections contained in these Design Capacity Tables. The signature curves were produced in the Thin-Wall buckling analysis program developed by The University of Sydney, and form the basis of design using the Direct Strength Method (DSM). They are included here to provide a clear picture of the buckling behaviour of the sections under the following loading conditions:
axial compression
bending about the $x$-axis
bending about the $y$-axis (lips in compression)
bending about the $y$-axis (web in compression)

DESIGN CAPACITY TABLES for $64 \times 41$ Lipped Channels to AS/NZS 4600

Graph A. 1

## SIGNATURE CURVE

$64 \times 41 \times 1.55$ LC
Axial Compression


Graph A. 2
SIGNATURE CURVE
$64 \times 41 \times 1.55$ LC
Bending about $x$-axis


## Graph A. 3



Graph A. 4

Bending about $y$-axis
(Web in Compression)


## Graph A. 5



Graph A. 6 SIGNATURE CURVE $64 \times 41 \times 1.15$ LC Bending about $x$-axis


Graph A. 7

## SIGNATURE CURVE

$64 \times 41 \times 1.15$ LC
Bending about $y$-axis
(Lips in Compression)


Graph A. 8 SIGNATURE CURVE
$64 \times 41 \times 1.15$ LC
Bending about $y$-axis (Web in Compresssion)


Graph A. 9


Graph A. 10
SIGNATURE CURVE
$64 \times 41 \times 0.95$ LC
Bending about $x$-axis


Graph A. 11



Graph A. 13

## SIGNATURE CURVE

$64 \times 41 \times 0.75$ LC
Axial Compression


Graph A. 14
SIGNATURE CURVE
$64 \times 41 \times 0.75$ LC
Bending about $x$-axis


Graph A. 15


Graph A. 16
SIGNATURE CURVE
$64 \times 41 \times 0.75$ LC
Bending about $y$-axis (Web in Compression)



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