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# **DESIGN CAPACITY TABLES**

for 89 x 41 Lipped Channels - Nestable to

# AS/NZS 4600

Version 02 January 2019

www.howickltd.com

#### Howick Ltd

Design Capacity Tables for 89 x 41 Lipped Channels - Nestable to AS/NZS 4600

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Users of this publication should note that the design capacities, calculations, tabulations and other information contained in this publication are specifically relevant to cold-formed steel sections manufactured on Howick roll-forming machines.

Consequently, the information contained in this publication cannot be readily used for coldformed sections produced on machines by other manufacturers, as those sections may vary significantly in geometry and material Standard compliance.

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## **About Howick Ltd**

Howick Ltd is a well-established and respected, 35 year, family enterprise based in Auckland, New Zealand.

Howick Ltd personifies the concept of "Kiwi ingenuity" showcasing technical experties and creativity and that essential "can do" philosophy that underpins the company's world-leading innovation and quality. Given this success, Howick Ltd is often described as producers of "the world's best steel framing machines".

We are a design and manufacturing company with a global philosophy and reach. Our emphasis is on unique research and development and sophisticated design technology enabling cost-effective, efficient end to end construction systems, across a variety of steel framed projects.

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09/01/2019

#### Howick Ltd

117 Vincent Street, Howick Auckland, New Zealand 2014

RE: DESIGN CAPACITY TABLES for 89 x 41 Lipped Channel Nestable to AS/NZS 4600:2018 Version 02 January 2019

#### Att: Nick Coubray,

As requested, Engineering Design Global Enterprise (EDGE Consulting Engineers), has undertaken a peer review of the documentation provided by Howick Ltd for the 89 x 41 Lipped Channel Nestable Sections as manufactured by Howick LTD. EDGE has been provided with the following documents:

- "Howick 89 x 41 LCN - DCT [2] 2018-10-24" and associated calculations.

- "89x41 LCN Properties & Capacities v08.xlsx"
- "89x41 LCN Lips Removed Properties & Capacities v06.xlsx"

These documents have been technically reviewed against the relevant standards.

The design capacity tables provided have been compared to the results within the reviewed spreadsheets and calculations and reviewed in accordance with AS/NZS 4600:2018. All calculations and capacity tables comply with AS/NZS 4600:2018.

Yours faithfully,

Inkt

TIM Peters BEng Meng MIEAust CPEng 67334 RBP RPEQ 5496 MIPENZ MIEPNG **© Howick Ltd** 

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## **Notations & Abbreviations**

Symbol	Description
Ag	gross area of a cross-section
b	flat width of a flange excluding radii
b <sub>f1</sub>	overall width of the larger flange
b <sub>f2</sub>	overall width of the smaller flange
$C_{ m b}$	bending coefficient dependent on moment
Cs	coefficient for moment about the cnetroidal axis perpendicular to the symmetry axis
C <sub>TF</sub>	coefficient for unequal end moment
С	distance from the end of a beam to the edge of the bearing force
d	overall depth of a section
<i>d</i> <sub>1</sub>	depth of the flat portion of a web measured along the plane of the web
$d_{L}$	overall depth of a lip
E	Young's modulus of elasticity
EOF	End One Flange (concentrated load or reaction on a beam)
ETF	End Two Flange (concentrated load or reaction on a beam)
f <sub>u</sub>	minimum tensile strength used in design
fy	minimum yield stress used in design
G	shear modulus of elasticity
I <sub>w</sub>	warping constant for a cross-section
l <sub>x</sub>	second moment of area about the major principal x-axis
l <sub>y</sub>	second moment of area about the minor principal y-axis
IOF	Interior One Flange (concentrated load or reaction on a beam)
ITF	Interior Two Flange (concentrated load or reaction on a beam)
J	torsion constant for the cross-section
L <sub>b</sub>	actual length of bearing
L <sub>e</sub>	effective length of a member
L <sub>ex</sub>	effective length for buckling about the major principal x-axis
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis

Symbol	Description
<i>M</i> *	design bending moment
<i>M</i> <sub>x</sub> *	design bending moment about the x-axis
<i>M</i> <sub>y</sub> *	design bending moment about the y-axis
Mb	nominal member moment capacity
M <sub>bdx</sub>	nominal moment capacity about the x-axis for distortional buckling
M <sub>bdyL</sub>	nominal moment capacity about the y-axis for distortional buckling (lips in compression)
<i>M</i> <sub>bdyW</sub>	nominal moment capacity about the y-axis for distortional buckling (web in compression)
M <sub>bx</sub>	nominal member moment capacity about the x-axis
M <sub>by</sub>	nominal member moment capacity about the y-axis
M <sub>byL</sub>	nominal member moment capacity about the y-axis (lips in compression)
M <sub>byW</sub>	nominal member moment capacity about the y-axis (web in compression)
M <sub>sx</sub>	nominal section moment capacity about the x-axis
M <sub>sxf</sub>	nominal yield moment capacity about the x-axis
M <sub>syfL</sub>	nominal yield moment capacity about the y-axis (tension in the lips)
M <sub>syfT</sub>	nominal yield moment capacity about the y-axis (tension in the toes)
M <sub>syfW</sub>	nominal yield moment capacity about the y-axis (tension in the web)
M <sub>syL</sub>	nominal section moment capacity about the y-axis (lips in compression)
M <sub>syT</sub>	nominal section moment capacity about the y-axis (toes in compression)
M <sub>syW</sub>	nominal section moment capacity about the y-axis (web in compression)
My	moment causing initial yield at the extreme compression fibre of a full section
N*	design axial force (tension or compression)
N <sub>c</sub>	nominal member capacity of a member in compression
N <sub>cd</sub>	nominal capacity of a member in compression for distortional buckling
N <sub>ex</sub>	elastic buckling load about the major principal x-axis
N <sub>ey</sub>	elastic buckling load about the minor principal y-axis
Ns	nominal section capacity of a member in compression



Symbol	Description		
Nt	nominal section capacity of a member in tension	]	
r <sub>i</sub>	inside corner radius	1	
r <sub>o1</sub>	polar radius of gyration of the cross-section about the shear centre	1	
r <sub>x</sub>	radius of gyration about the major principal x-axis	1	
r <sub>y</sub>	radius of gyration about the minor principal y-axis		
t	nominal base metal thickness of a section exclusive of coatings	1	
V <sub>vx</sub>	nominal shear capacity of the cross-section perpendicular to the x-axis	1	
V <sub>vy</sub>	nominal shear capacity of the cross-section perpendicular to the x-axis		
V <sub>x</sub> *	design shear force		
V <sub>y</sub> *	design shear force		
w <sub>h</sub>	total hole width		
X	major principal axis of the cross-section		
x <sub>c</sub>	co-ordinate of the centroid from the back of the web along the x-axis		
x <sub>o</sub>	co-ordinate of the shear centre from the centroid along the x-axis		
У	minor principal axis of the cross-section		
Z <sub>x</sub>	elastic section modulus about the major principal x-axis		
Z <sub>yL</sub>	elastic section modulus about the minor principal y-axis (lips in compression)		
Z <sub>yW</sub>	elastic section modulus about the minor principal y-axis (web in compression)	]	
ατ	coefficient of thermal expamsion	1	
βγ	monosymmetry section constant about the y-axis		
φ <sub>b</sub>	capacity reduction factor for bending		
φc	capacity reduction factor for compression		
φ <sub>t</sub>	capacity reduction factor for tension		
φ <sub>v</sub>	capacity reduction factor for shear		
φ <sub>w</sub>	capacity reduction factor for bearing	vick	
ν	Poisson's ratio (= 0.3 for steel)		
ρ	density of steel	]	

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DESIGN CAPACITY TABLES for 89 x 41 Lipped Channels - Nestable to AS/NZS 4600

#### INTRODUCTION

#### Scope

These Design Capacity Tables have been prepared for the following nestable lipped channel cold-formed sections manufactured on Howick Ltd. steel roll-forming machines.

89 x 41 x 1.55 LCN 89 x 41 x 1.15 LCN 89 x 41 x 0.95 LCN 89 x 41 x 0.75 LCN

The values presented in the tables and graphs are only applicable to sections manufactured on Howick Ltd. machines, and for the specified steel grades complying with AS 1397.

All of the dimensions and section properties required for design are provided, as well as design aids in the form of tables and graphs for members subject to the following design actions:

Bending Axial Compression Axial Tension Combined Actions

These design aids will allow engineers to design most structures without having to refer to the design standard AS/NZS 4600.

#### **Design Method**

The Tables and Graphs in this publication have been calculated generally in accordance with the Australian and New Zealand standard AS/NZS 4600 Cold-Formed steel Structures. The Direct Strength Method (DSM) has been used to determine the capacities for axial compression and bending, based on the results of finite strip analyses using the computer program "Thin-Wall" from The University of Sydney.

Where appropriate, the method of calculating capacities in the transition region between local and distortional buckling in accordance with the AISI publication "Direct Strength Mothod" has been used. This is an extension of what is given in AS/NZS 4600.

#### Limit States Design

All values presented in these Design Capacity Tables are limit state values in accordance with the Limits State Design requirements of AS/NZS 4600 and AS/NZS 1170.0.

#### Units

The units in the Tables are consistent with those in the SI (metric) system. The base units used in the tables and graphs are:

Property	Units	Symbol
Force	Newton	Ν
Length	metre	m
Mass	kilogram	kg
Stress	Megapascal	MPa

Except for some minor exceptions, all values in the Tables are rounded to three (3) significant figures.

#### **Properties of Steel**

The properties of steel used for the calculation of capacities in these Tables are given in the table below. The coefficient of expansion for steel is also listed.

Property	Symbol	Value
Young's Modulus of Elasticity	E	200 x 10 <sup>3</sup> MPa
Shear Modulus	G	80 x 10 <sup>3</sup> MPa
Poisson's Ratio	ν	0.3
Density	ρ	7850 kg/m <sup>3</sup>
Coefficient of Thermal Expansion	ατ	11.7 x 10 <sup>-6</sup> per °C

The steel grades and mechanical properties used for design in accordance with AS/NZS 4600 are given in the table below. Note that the yield stress and tensile strength for thin sections of Grade G550 steel are reduced as required by this standard.

Section	Grade	Yield Stress f <sub>y</sub> (MPa)	Tensile Strength f <sub>u</sub> (MPa)
89 x 41 x 1.55 LCN	G450	450	480
89 x 41 x 1.15 LCN	G500	500	520
89 x 41 x 0.95 LCN	G550	550	550
89 x 41 x 0.75 LCN	G550	495	495



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#### References

#### **Referenced Standards**

AS 1397-2011, Continuous hot-dip metallic coated steel sheet and strip - Coatings of zinc and zinc alloyed with aluminium and magnesium, Standards Australia

AS/NZS 1170.1: 2002, Structural Design Actions Part 0: General Principles, Standards Australia.

AS/NZS 4600: 2018, Cold-Formed Steel Structures, Standards Australia.

**Other References** 

AISI 2006, Direct Strength Method (DSM) Design Guide, American Iron and Steel Institute, January 2006.

Centre of Advanced Structural Engineering (CASE) 2001, "THIN-WALL", Computer Program.

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 Dimensions & Section Properties

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# Part 1: Dimensions & Section Properties

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# **DIMENSIONS & SECTION PROPERTIES**



		DI	MENSIC	NS					SECTION PROPERTIES										
Designation	Depth	Large Flange Width	Small Flange Width	Lip Depth	Thick.	Inside Co-ord. Gross hick. Corner of Mass Section About x-axis Radius Centroid per Area metre				About	y-axis								
	d	b <sub>f1</sub>	b <sub>f2</sub>	$d_{L}$	t	<i>r</i> i	Xc		Ag	l <sub>x</sub>	Z <sub>x</sub>	r <sub>x</sub>	l <sub>y</sub>	$Z_{\rm yL}$	$Z_{yW}$	ry			
	mm	mm	mm	mm	mm	mm	mm	kg/m	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm			
89 x 41 x 1.55 LCN - G450	89.0	41.3	39.0	10.0	1.55	1.5	12.6	2.18	278	0.347	7.81	35.4	0.0584	2.12	4.62	14.5			
89 x 41 x 1.15 LCN - G500	89.0	41.3	39.0	10.0	1.15	1.5	12.6	1.64	208	0.264	5.92	35.6	0.0450	1.63	3.55	14.7			
89 x 41 x 0.95 LCN - G550	89.0	41.3	39.0	10.0	0.95	1.5	12.6	1.36	173	0.220	4.95	35.7	0.0378	1.38	2.99	14.8			
89 x 41 x 0.75 LCN - G550	89.0	41.3	39.0	10.0	0.75	1.5	12.7	1.08	137	0.176	3.95	35.8	0.0304	1.11	2.40	14.9			

NOTES:

1. Calculations of section properties are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Properties are calculated for an equal flange lipped channel using the average flange width.

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# SECTION PROPERTIES TO CALCULATE MEMBER STABILITY



DIMENSIONS										RATIOS PROPERTIES						MATERIAL			
Designation	Depth	Large Flange Width	Small Flange Width	Lip Depth	Thick- ness	Inside Corner Radius	Flat Web Depth	Flat Flange Width	Mass per metre	Web	Flange	Shear Centre Co-ord.	Polar Rad. of Gyration about S.C.	Mono- Symmetry Constant	Torsion Constant	Warping Constant	Grade	Design Yield Stress	Design Tensile Strength
	d	b <sub>f1</sub>	b <sub>f2</sub>	dL	t	r <sub>i</sub>	d <sub>1</sub>	b	mouro	d <sub>1</sub> /t	b/t	x <sub>o</sub>	r <sub>o1</sub>	β <sub>y</sub>	J	I <sub>w</sub>		f <sub>y</sub>	f <sub>u</sub>
	mm	mm	mm	mm	mm	mm	mm	mm	kg/m			mm	mm		mm <sup>4</sup>	10 <sup>6</sup> mm <sup>6</sup>		MPa	MPa
89 x 41 x 1.55 LCN - G450	89.0	41.3	39.0	10.0	1.55	1.5	82.9	34.1	2.18	53.5	22.0	30.1	48.7	101	222	96.0	G450	450	480
89 x 41 x 1.15 LCN - G500	89.0	41.3	39.0	10.0	1.15	1.5	83.7	34.9	1.64	72.8	30.3	30.6	49.1	101	91.8	74.6	G500	500	520
89 x 41 x 0.95 LCN - G550	89.0	41.3	39.0	10.0	0.95	1.5	84.1	35.3	1.36	88.5	37.1	30.8	49.4	102	52.0	63.1	G550	550	550
89 x 41 x 0.75 LCN - G550	89.0	41.3	39.0	10.0	0.75	1.5	84.5	35.7	1.08	113	47.5	31.0	49.6	102	25.7	50.9	G550	495	495

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. The flat flange width is the average of the flanges.
- 6. Properties are calculated for an equal flange lipped channel using the average flange width.





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#### Part 2: Members subject to Bending

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#### Table 2.1

# **MEMBER MOMENT CAPACITY**

Members without Full Lateral Restraint

bending about x-axis

 $C_{\rm b} = 1.0$ 



	Mass	Buckling Capacities		uckling Capacities Design Member Moment Capacity, $\phi_b M_{bx}$ (kNm)													
Designation	per	Local	Distortional														
Designation	metre	$\phi_{\sf b} M_{\sf sx}$	$\phi_{\rm b} M_{\rm bdx}$						Effec	tive Lengt	h (L <sub>e</sub> ) in m	netres					
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3	3.3	3.6	4
89 x 41 x 1.55 LCN - G450	2.18	3.16	2.81	2.96	2.81	2.81	2.81	2.52	2.01	1.48	1.13	0.907	0.749	0.635	0.549	0.483	0.416
89 x 41 x 1.15 LCN - G500	1.64	2.56	2.03	2.39	2.03	2.03	2.03	2.02	1.52	1.08	0.815	0.641	0.521	0.435	0.371	0.322	0.273
89 x 41 x 0.95 LCN - G550	1.36	2.01	1.65	2.01	1.66	1.65	1.65	1.62	1.26	0.892	0.667	0.520	0.420	0.348	0.294	0.253	0.212
89 x 41 x 0.75 LCN - G550	1.08	1.27	1.12	1.27	1.17	1.12	1.12	1.07	0.878	0.690	0.524	0.406	0.325	0.267	0.225	0.192	0.159

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for a uniform bending moment ( $C_{\rm b}$  = 1.0).
- 6. Refer to Graph 2.1 for the limits of the local and distortional design moment capacities.
- 7. The effective length  $L_{\rm e} = L_{\rm ey} = L_{\rm ez}$ .
- 8. Capacities are calculated for an equal flange lipped channel using the average flange width. HOWICK Ltd



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Graph 2.1

## MEMBER MOMENT CAPACITY



Members without Full Lateral Restraint

#### bending about x-axis

 $C_{\rm b} = 1.0$ 



#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for a uniform bending moment ( $C_{\rm b}$  = 1.0).
- 6. The effective length  $L_{\rm e} = L_{\rm ey} = L_{\rm ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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# $t \rightarrow b_{f1}$

#### Table 2.2

# MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

bending about y-axis

(Lips in Compression)



Tension

	Mass	Buckling (	Buckling Capacities			Buckling Capacities Design Member Moment Capacity, $\phi_{\rm b} M_{\rm byL}$ (kNm)														
Designation	per	Local	Distortional																	
Designation	metre	$\phi_{\sf b}  M_{\sf syL}$	$\phi_{\sf b}  M_{\sf bdyL}$						Effec	tive Lengt	h (L <sub>e</sub> ) in m	etres								
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0			
89 x 41 x 1.55 LCN - G450	2.18	0.860	0.804	0.860	0.804	0.804	0.804	0.780	0.697	0.609	0.520	0.436	0.375	0.332	0.299	0.274	0.249			
89 x 41 x 1.15 LCN - G500	1.64	0.736	0.590	0.736	0.594	0.590	0.590	0.590	0.551	0.450	0.351	0.283	0.236	0.203	0.178	0.159	0.140			
89 x 41 x 0.95 LCN - G550	1.36	0.681	0.486	0.681	0.511	0.486	0.486	0.486	0.477	0.366	0.278	0.221	0.182	0.154	0.133	0.117	0.102			
89 x 41 x 0.75 LCN - G550	1.08	0.483	0.330	0.483	0.372	0.330	0.330	0.330	0.330	0.283	0.213	0.167	0.136	0.113	0.0964	0.0838	0.0711			

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. Refer to Graph 2.2 for the limits of the local and distortional design moment capacities.
- 7. The effective length  $L_{\rm e} = L_{\rm ex} = L_{\rm ez}$ .
- 8. Capacities are calculated for an equal flange lipped channel using the average flange width.





## Graph 2.2

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

#### bending about y-axis

(Lips in Compression)







#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. The effective length  $L_{e} = L_{ex} = L_{ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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# $t \rightarrow b_{f_2}$

#### Table 2.3

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

bending about y-axis

(Web in Compresion)



	Mass	Buckling (	kling Capacities Design Member Moment Capacity, $\phi_b M_{byW}$ (kNm)														
Designation	per	Local	Distortional														
Designation	metre	$\phi_{\sf b} M_{\sf syW}$	$\phi_{\rm b}  M_{ m bdyW}$						Effec	tive Lengt	h (L <sub>e</sub> ) in m	netres					
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	0.846	N.A.	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846
89 x 41 x 1.15 LCN - G500	1.64	0.574	N.A.	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574
89 x 41 x 0.95 LCN - G550	1.36	0.450	N.A.	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450
89 x 41 x 0.75 LCN - G550	1.08	0.286	N.A.	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. Refer to Graph 2.3 for the limits of the local and distortional design moment capacities.
- 7. The effective lengths  $L_e = L_{ex} = L_{ez}$ .
- 8. Capacities are calculated for an equal flange lipped channel using the average flange width.



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Graph 2.3

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

#### bending about y-axis

(Web in Compression)







- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. The effective length  $L_{e} = L_{ex} = L_{ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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#### Table 2.4

# **SHEAR CAPACITIES**



	Mass	Shear C	Capacity
Designation	per	x-axis	y-axis
Doorgination	metre	$\phi_{v} V_{vx}$	$\phi_{v} V_{vy}$
	kg/m	kN	kN
89 x 41 x 1.55 LCN - G450	2.18	30.3	27.4
89 x 41 x 1.15 LCN - G500	1.64	15.8	23.1
89 x 41 x 0.95 LCN - G550	1.36	8.87	21.2
89 x 41 x 0.75 LCN - G550	1.08	4.34	14.9

#### NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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# Graph 2.4

# **COMBINED BENDING & SHEAR**





#### 35 89 x 41 x 1.55 LCN - G450 30 25 Design Shear Force $V_x^*$ (kN) 20 89 x 41 x 1.15 LCN - G500 15 89 x 41 x 0.95 LCN - G550 10 89 x 41 x 0.75 LCN - G550 5 0 0 0.5 1.5 1.0 2.0 2.5 3.0 3.5

Design Bending Moment  $M_{x}^{*}$  (kNm)

#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.



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# **COMBINED BENDING & SHEAR**

**bending about y-axis** (Lips in Compression)

Graph 2.5





30 25 89 x 41 x 1.55 LCN - G450 20 89 x 41 x 1.15 LCN - G500 89 x 41 x 0.95 LCN - G550 10 89 x 41 x 0.75 LCN - G550

#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.



0.1

0.2

0.3

0.4

0.5

Design Bending Moment  $M_v^*$  (kNm)

0.6

Design Shear Force  $V_y^*$  (kN)

5

0 0

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0.7

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0.8

0.9



# **COMBINED BENDING & SHEAR**

bending about y-axis (Web in Compression)

Graph 2.6







- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.



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#### Table 2.5

# WEB BEARING CAPACITY

One Flange Loading or Reaction



End Bearing ( $c < 1.5 d_1$ )

Interior Bearing ( $c \ge 1.5 d_1$ )

	Mass						Design W	eb Bearing	Capacity, o	∳ <sub>w</sub> R <sub>bx</sub> (kN)				
Designation	per	1.5 d <sub>1</sub>			End Bearing	g (c < 1.5 d <sub>1</sub> )					Interior Bearing	ng (c $\geq$ 1.5 d <sub>1</sub> )	)	
Designation	metre				Bearing Len	igth, L <sub>b</sub> (mm)					Bearing Len	igth, <i>L</i> <sub>b</sub> (mm)		
	kg/m	mm	25	50	75	100	125	150	25	50	75	100	125	150
89 x 41 x 1.55 LCN - G450	2.18	124.4	6.13	7.61	8.75	9.71	10.6	11.3	14.2	16.3	17.9	19.3	20.5	21.6
89 x 41 x 1.15 LCN - G500	1.64	125.6	3.88	4.88	5.64	6.29	6.85	7.37	8.62	10.0	11.1	12.0	12.8	13.6
89 x 41 x 0.95 LCN - G550	1.36	126.2	2.97	3.76	4.37	4.88	5.33	5.74	6.43	7.54	8.39	9.11	9.75	10.3
89 x 41 x 0.75 LCN - G550	1.08	126.8	1.70	2.17	2.53	2.84	3.11	3.35	3.55	4.21	4.72	5.14	5.52	5.85

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Capacities are calculated for an equal flange lipped channel using the average flange width.



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#### Table 2.6

# WEB BEARING CAPACITY

Two Flange Loading or Reaction



	Mass						Design V	Veb Bearing	Capacity,	$\phi_w R_{bx} (kN)$				
Designation	per	1.5 d <sub>1</sub>			End Bearing	g (c < 1.5 d <sub>1</sub> )	1				Interior Beari	ng (c $\geq$ 1.5 d <sub>1</sub> )	)	
Designation	metre				Bearing Len	igth, L <sub>b</sub> (mm)	)				Bearing Ler	ngth, <i>L</i> <sub>b</sub> (mm)		
	kg/m	mm	25	50	75	100	125	150	25	50	75	100	125	150
89 x 41 x 1.55 LCN - G450	2.18	124.4	7.36	7.87	8.26	8.59	8.89	9.15	16.1	18.6	20.6	22.2	23.6	24.9
89 x 41 x 1.15 LCN - G500	1.64	125.6	3.99	4.30	4.54	4.74	4.92	5.08	8.69	10.2	11.3	12.3	13.1	13.9
89 x 41 x 0.95 LCN - G550	1.36	126.2	2.72	2.95	3.13	3.28	3.41	3.53	5.79	6.83	7.63	8.31	8.90	9.44
89 x 41 x 0.75 LCN - G550	1.08	126.8	1.32	1.45	1.54	1.62	1.69	1.75	2.61	3.11	3.50	3.82	4.11	4.37

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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#### Part 3: Members subject to Axial Compression

Table 3.1:Axial Compression CapacityGraph 3.1:Axial Compression Capacity

# Part 3: Members subject to Axial Compression

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# AXIAL COMPRESSION CAPACITY

Table 3.1

 $L_{\rm ex} = L_{\rm ey} = L_{\rm ez}$ 



	Mass	Buckling (	Capacities					Design A	Axial Co	mpressi	on Capa	ιcities, φ <sub>α</sub>	N <sub>c</sub> (kN)				
Designation	per	Local	Distortional														
Doorgnation	metre	$\phi_{\rm c} N_{\rm s}$	$\phi_{\rm c} N_{\rm cd}$						Effec	tive Lengt	th (L <sub>e</sub> ) in m	etres					
	kg/m	kN	kN	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	80.4	74.7	78.9	77.2	68.6	56.9	44.3	30.3	22.6	17.9	14.8	11.8	9.55	7.89	6.63	5.37
89 x 41 x 1.15 LCN - G500	1.64	52.3	50.4	51.3	50.1	44.1	35.8	26.9	20.4	15.4	11.9	9.55	7.96	6.82	5.98	5.10	4.13
89 x 41 x 0.95 LCN - G550	1.36	40.2	39.5	39.4	38.4	33.4	26.6	19.5	14.7	11.7	9.37	7.44	6.11	5.17	4.46	3.93	3.39
89 x 41 x 0.75 LCN - G550	1.08	25.1	25.9	24.6	24.0	21.2	17.3	13.0	9.83	7.82	6.44	5.46	4.54	3.78	3.22	2.79	2.37

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Refer to Graph 3.1 for the limits of the local and distortional design moment capacities.
- 6. The effective length  $L_{e} = L_{ex} = L_{ey} = L_{ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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# Part 4: Members subject to Axial Tension

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Part 4: Members subject to Axial Tension

 Table 4.1:
 Axial Tension Capacity



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Table 4.1

# **AXIAL TENSION CAPACITIES**

with and without holes



	Mass						Design A	xial Tens	ion Capa	city, $\phi_t N_t$	(kN)					
Designation	per	Uniform			We	eb Connect	ed					Both F	langes Con	nected		
Designation	metre	Tension			Total h	ole Width, v	<i>w</i> <sub>h</sub> (m)					Total h	nole Width,	w <sub>h</sub> (m)		
	kg/m	(NO Holes)	0	10	20	25	30	35	40	0	10	20	25	30	35	40
89 x 41 x 1.55 LCN - G450	2.18	112.5	86.7	81.9	77.0	74.6	72.2	69.8	67.3	86.7	81.9	77.0	74.6	72.2	69.8	67.3
89 x 41 x 1.15 LCN - G500	1.64	93.7	70.4	66.5	62.7	60.7	58.8	56.8	54.9	70.4	66.5	62.7	60.7	58.8	56.8	54.9
89 x 41 x 0.95 LCN - G550	1.36	85.6	61.9	58.5	55.1	53.4	51.7	50.0	48.3	61.9	58.5	55.1	53.4	51.7	50.0	48.3
89 x 41 x 0.75 LCN - G550	1.08	61.2	44.2	41.8	39.4	38.2	37.0	35.7	34.5	44.2	41.8	39.4	38.2	37.0	35.7	34.5

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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#### Part 5: Members subject to Combined Actions

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Table 5.2:	Elastic Buckling Load (x-axis)
Table 5.3:	Elastic Buckling Load (y-axis)

# Part 5: Members subject to Combined Actions

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# **SECTION & YIELD CAPACITIES**

Table 5.1



	Mass	Design Sectior	Axial Capacities	Design S	Section Moment C	apacities	Design Yield	Moment Capacit	ties (Tension)
Designation	maoo	Tension	Compression	about x-axis	about	y-axis	about x-axis	about	y-axis
Designation	per m	$\phi_t N_t$	$\phi_c N_s$	$\phi_b M_{sx}$	$\phi_{\sf b} M_{\sf syL}$	$\phi_{\sf b} M_{\sf syW}$	$\phi_{\rm b}M_{\rm sxf}$	$\phi_{\sf b} M_{\sf syfL}$	$\phi_{\sf b} M_{\sf syfW}$
	kg/m	kN	kN	kNm	kNm	kNm	kNm	kNm	kNm
89 x 41 x 1.55 LCN - G450	2.18	112	80.4	3.16	0.860	0.846	3.16	0.860	1.87
89 x 41 x 1.15 LCN - G500	1.64	93.7	52.3	2.56	0.736	0.574	2.67	0.736	1.60
89 x 41 x 0.95 LCN - G550	1.36	85.6	40.2	2.01	0.681	0.450	2.45	0.681	1.48
89 x 41 x 0.75 LCN - G550	1.08	61.2	25.1	1.27	0.483	0.286	1.76	0.493	1.07

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5.  $\phi_b M_{syL}$  and  $\phi_b M_{syW}$  refer to bending about the y-axis causing compression in the lips and web of the channel respectively.
- φ<sub>b</sub>M<sub>syfL</sub> and φ<sub>b</sub>M<sub>syfW</sub> are the design yield moments for bending about the y-axis causing tension in the lips and web of the channel respectively.
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.





Table 5.2

## **ELASTIC BUCKLING LOAD**

buckling about x-axis

	Mass						Elast	ic Buckling	g Load, N <sub>e</sub>	<sub>x</sub> (kN)					
Designation	metre							Effective Le	ngth, <i>L<sub>ex</sub> (</i> m)						
	kg/m	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	17147	7621	1905	847	476	305	212	156	119	94.1	76.2	63.0	52.9	42.9
89 x 41 x 1.15 LCN - G500	1.64	13006	5781	1445	642	361	231	161	118	90.3	71.4	57.8	47.8	40.1	32.5
89 x 41 x 0.95 LCN - G550	1.36	10863	4828	1207	536	302	193	134	98.5	75.4	59.6	48.3	39.9	33.5	27.2
89 x 41 x 0.75 LCN - G550	1.08	8670	3853	963	428	241	154	107	78.6	60.2	47.6	38.5	31.8	26.8	21.7

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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Table 5.3

## **ELASTIC BUCKLING LOAD**

buckling about y-axis

	Mass						Elast	ic Buckling	Load, N <sub>e</sub>	<sub>y</sub> (kN)					
Designation	metre							Effective Ler	ngth, <i>L<sub>ey</sub> (</i> m)						
	kg/m	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	2882	1281	320	142	80.1	51.2	35.6	26.1	20.0	15.8	12.8	10.6	8.89	7.20
89 x 41 x 1.15 LCN - G500	1.64	2218	986	246	110	61.6	39.4	27.4	20.1	15.4	12.2	9.86	8.15	6.85	5.55
89 x 41 x 0.95 LCN - G550	1.36	1866	830	207	92.2	51.8	33.2	23.0	16.9	13.0	10.2	8.30	6.86	5.76	4.67
89 x 41 x 0.75 LCN - G550	1.08	1501	667	167	74.1	41.7	26.7	18.5	13.6	10.4	8.23	6.67	5.51	4.63	3.75

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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- Table 6.2 Section Properties to Calculate Member Stability
- Table 6.3: Section & Yield Capacities
- Table 6.4: Axial Compression Capacity
- Graph 6.1: Combined Bending & Shear (bending about y-axis)

# Part 6: MEMBERS with LIPS REMOVED

### GENERAL

When these lipped channel sections are used in frames and trusses, there will be instances where the lips of the sections are removed at the location of the connections. This part of the document provides design tables and graphs which will aid in the design of the unlipoped sections produced by removing the lips. The diagram below illustrates the portion of the section which is removed.

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DESIGN CAPACITY TABLES for 89 x 41 Lipped Channels - Nestable to AS/NZS 4600

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### Table 6.1



# **DIMENSIONS & SECTION PROPERTIES**

Lips Removed



	DIMENSIONS           Designation         Large Midth         Small Flange Flange Width         Inside Co-ord. Corner Radius         Co-ord. of Centroid           d         b <sub>f1</sub> b <sub>f2</sub> t         r <sub>1</sub> x <sub>c</sub> mm         mm         mm         mm         mm         mm         mm           41 x 1.55 LCN-LR - G450         89.0         38.3         36.0         1.55         1.50         9.12           41 x 1.15 LCN-LR - G500         89.0         38.7         36.4         1.15         1.50         9.10									SE		ROPERTIE	ES		
Designation	Depth	Large Flange Width	Small Flange Width	Thick.	Inside Corner Radius	Co-ord. of Centroid	Mass per metre	Gross Section Area		About x-axis			About	y-axis	
	d	b <sub>f1</sub>	b <sub>f2</sub>	t	r <sub>i</sub>	xc	mouro	Ag	l <sub>x</sub>	Z <sub>x</sub>	r <sub>x</sub>	l <sub>y</sub>	$Z_{\rm yL}$	$Z_{yW}$	ry
	mm	mm	mm	mm	mm	mm	kg/m	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm
89 x 41 x 1.55 LCN-LR - G450	89.0	38.3	36.0	1.55	1.50	9.12	1.92	245	0.296	6.65	34.7	0.0325	1.161	3.56	11.5
89 x 41 x 1.15 LCN-LR - G500	89.0	38.7	36.4	1.15	1.50	9.10	1.44	184	0.225	5.05	35.0	0.0252	0.889	2.77	11.7
89 x 41 x 0.95 LCN-LR - G550	89.0	38.9	36.6	0.95	1.50	9.09	1.20	153	0.188	4.22	35.1	0.0213	0.745	2.34	11.8
89 x 41 x 0.75 LCN-LR - G550	89.0	39.1	36.8	0.75	1.50	9.09	0.952	121	0.150	3.37	35.2	0.0172	0.598	1.90	11.9

NOTES:

1. Calculations of section properties are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Properties are calculated for an equal flange lipped channel using the average flange width.

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#### Table 6.2



# SECTION PROPERTIES TO CALCULATE MEMBER STABILITY

Lips Removed



		DIME	ENSION	S					RA	rios		PF	ROPERTIE	S		M	ATERIA	۹L
Designation	Depth	Large Flange Width	Small Flange Width	Thick- ness	Inside Corner Radius	Flat Web Depth	Flat Flange Width	Mass per metre	Web	Flange	Shear Centre Co-ord.	Polar Rad. of Gyration about S.C.	Mono- Symmetry Constant	Torsion Constant	Warping Constant	Grade	Design Yield Stress	Design Tensile Strength
-	d	b <sub>f1</sub>	b <sub>f2</sub>	t	r <sub>i</sub>	d <sub>1</sub>	b	metre	d <sub>1</sub> /t	b/t	x <sub>o</sub>	r <sub>01</sub>	β <sub>y</sub>	J	I <sub>w</sub>		f <sub>y</sub>	f <sub>u</sub>
	mm	mm	mm	mm	mm	mm	mm	kg/m			mm	mm		mm <sup>4</sup>	10 <sup>6</sup> mm <sup>6</sup>		MPa	MPa
89 x 41 x 1.55 LCN-LR - G450	89.0	38.3	36.0	1.55	1.50	82.9	34.1	1.92	53.5	22.0	21.2	42.3	98.3	196.3	44.0	G450	450	480
89 x 41 x 1.15 LCN-LR - G500	89.0	38.7	36.4	1.15	1.50	83.7	34.9	1.44	72.8	30.3	21.7	42.8	98.9	81.1	34.5	G500	500	520
89 x 41 x 0.95 LCN-LR - G550	89.0	38.9	36.6	0.95	1.50	84.1	35.3	1.20	88.5	37.1	21.9	43.0	99.2	46.0	29.3	G550	550	550
89 x 41 x 0.75 LCN-LR - G550	89.0	39.1	36.8	0.75	1.50	84.5	35.7	0.952	113	47.5	22.1	43.2	99.5	22.7	23.7	G550	495	495

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Properties are calculated for an equal flange lipped channel using the average flange width.

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# Table 6.3

## **SECTION & YIELD CAPACITIES**

Lips Removed



	Mass	Design Section	Axial Capacities	Design S	ection Moment C	Capacities	Design Yield	Moment Capacit	ies (Tension)
Designation	indee	Tension	Compression	about x-axis	about	y-axis	about x-axis	about	y-axis
Designation	per m	$\phi_t N_t$	$\phi_c N_s$	$\phi_b M_{sx}$	$\phi_{\sf b} M_{\sf syT}$	$\phi_{\sf b} M_{\sf syW}$	$\phi_{\sf b} M_{\sf sxf}$	$\phi_{\rm b}M_{\rm syfT}$	$\phi_{\sf b} M_{\sf syfW}$
	kg/m	kN	kN	kNm	kNm	kNm	kNm	kNm	kNm
89 x 41 x 1.55 LCN-LR - G450	1.92	99.3	61.4	2.01	0.400	0.470	2.69	0.470	1.44
89 x 41 x 1.15 LCN-LR - G500	1.44	82.8	39.5	1.31	0.265	0.352	2.27	0.400	1.25
89 x 41 x 0.95 LCN-LR - G550	1.20	75.6	30.2	1.01	0.205	0.277	2.09	0.369	1.16
89 x 41 x 0.75 LCN-LR - G550	0.952	54.0	18.7	0.629	0.129	0.176	1.50	0.266	0.844

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- φ<sub>b</sub>M<sub>syT</sub> and φ<sub>b</sub>M<sub>syW</sub> refer to bending about the y-axis causing compression in the toes and web of the channel respectively.
- 6.  $\phi_b M_{syfT}$  and  $\phi_b M_{syfW}$  are the design yield moment capacities for bending about the y-axis causing tension in the toes and web of the channel respectively.
- 7. All section moment capacities are applicable for unrestrained lengths up to 400 mm. Lips removed WICK \_\_\_\_\_\_ for more than this length is not expected.
- 8. Capacities are calculated for an equal flange channel using the average flange width.



# $t \rightarrow b_{f1}$

# AXIAL COMPRESSION CAPACITY

Table 6.4

 $L_{\text{ex}} = L_{\text{ey}} = L_{\text{ez}}$ Lips Removed



	Mass	Design Axial Compression Capacity, $\phi_c N_c$ (kN)								
Designation	per metre	Effective Length ( $L_{e}$ ) in metres								
	kg/m	0.0	0.10	0.20	0.30	0.35	0.40			
89 x 41 x 1.55 LCN-LR - G450	1.92	61.4	61.0	59.9	58.1	56.9	55.6			
89 x 41 x 1.15 LCN-LR - G500	1.44	39.5	39.3	38.5	37.2	36.4	35.5			
89 x 41 x 0.95 LCN-LR - G550	1.20	30.2	30.0	29.3	28.3	27.6	26.9			
89 x 41 x 0.75 LCN-LR - G550	0.952	18.7	18.6	18.3	17.7	17.3	16.9			

#### NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600.
- 5. Refer to Graph 3.1 for the limits of the local and distortional design moment capacities.
- 6. The effective length  $L_e = L_{ex} = L_{ey} = L_{ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.





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bending about y-axis

Lips Removed

Graph 6.1





Web in Compression





Tension

**Toes in Compression** 

DESIGN CAPACITY TABLES for 89 x 41 Lipped Channels - Nestable to AS/NZS 4600

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- Table 7.1: Wall stud Design Capacities Unclad
- Table 7.1: Wall stud Design Capacities Clad Both Sides
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# Part 7: Wall Framing Design Capacities

### GENERAL

This part of the Design Capacity tables provide capacities which may be used for the design of the sections as wall studs and wall plates. Three typical wall heights are specified for the wall studs.

The NASH wall stud and plate classifications for both Australia and New Zealand are also included in the tables for each section. These are based on the minimum properties and capacities given in the NASH references.

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# Table 7.1

# WALL STUD DESIGN CAPACITIES

Unclad



	Mass	Design Properties and Capacities										SH
Designation	per		Lateral	Actions		Compr	ession	Tension	Combine	d Actions	Wall Stud	
Doorgnation	metre	l <sub>x</sub>	$\phi_{\rm b}M_{\rm sx}$	$\phi_{\rm b} M_{\rm bx}$	$\phi_v V_{vx}$	$\phi_{\rm c} N_{\rm s}$	$\phi_{\rm c} N_{\rm c}$	$\phi_t N_t$	$\phi_{\sf b}M_{\sf sxf}$	N <sub>ex</sub>	Classi	lication
	kg/m	10 <sup>6</sup> mm <sup>4</sup>	kNm	kNm	kN	kN	kN	kN	kNm	kN	Australia	New Zealand
Stud Height 2440 mm												
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	49.6	86.7	3.16	144	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	30.8	70.4	2.67	108	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.87	40.2	22.6	61.9	2.45	89.6	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	15.0	44.2	1.76	71.1	SB	SB
Stud Height 2740 mm												
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	43.5	86.7	3.16	114	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	26.9	70.4	2.67	85.6	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.9	40.2	19.5	61.9	2.45	71.1	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	13.1	44.2	1.76	56.4	SB	SB
	Stud Height 3040 mm											
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	50.5	86.7	3.16	92.7	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	31.7	70.4	2.67	69.5	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.9	40.2	23.3	61.9	2.45	57.7	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	15.4	44.2	1.76	45.8	SB	SB



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#### Wall Stud Design Assumptions

Effective Lengths for Design								
Stud Height (mm)	2440	2740	3040					
No. of Noggings	1	1	2					
L <sub>ex</sub> (mm)	1952	2192	2432					
L <sub>ey</sub> (mm)	976	1096	810					
L <sub>ez</sub> (mm)	976	1096	810					

#### NOTES:

- 1. Noggings are equally spaced.
- 2. Lateral restraint is assumed to be provided by noggings only. Additional lateral restraint provided by cladding is ignored.
- 3. Both flanges of the stud are restrained by the top and bottom plates and the noggings.
- 4. Effective lengths are taken as 80% of the distance between restraints in accordance with NASH Handbook Clause 3.4.2.
- 5. No allowance has been made for holes in the web of the stud.

Symbol	Description
I <sub>x</sub>	second moment of area about the major principal x-axis
$\phi_{\rm c} N_{\rm s}$	design section capacity of a member in compression
$\phi_{c} N_{c}$	design member capacity of a member in compression
$\phi_{\rm b} M_{\rm sx}$	design section moment capacity about the x-axis
$\phi_{\sf b} M_{\sf bx}$	design member moment capacity about the x-axis
$\phi_{\sf b} M_{\sf sxf}$	design yield moment capacity about the x-axis
$\phi_{\rm v} V_{\rm vx}$	design shear capacity of the cross-section perpendicular to the x-axis
N <sub>ex</sub>	elastic buckling load about the major principal x-axis
$\phi_t N_t$	design section capacity of a member in tension
L <sub>ex</sub>	effective length for buckling about the major principal x-axis
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis

#### References

AS/NZS 4600 Cold-Formed Steel Structures.

NASH Standard (NZ), Residential and Low-Rise Steel Framing, Part 1: Design Criteria.

NASH Standard (Aust.), Residential and Low-Rise Steel Framing, Part 2: Design Solutions.

NASH Handbook (Aust.), Best Practice for Design and Construction of Residential and Low-Rise Steel Framing, Chapter 3.

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Table 7.2

# WALL STUD DESIGN CAPACITIES

Clad Both Sides



	Mass	Design Properties and Capacities										SH
Designation	per		Lateral	Actions		Compr	ession	Tension	Combine	d Actions	Wall Stud	
Designation	metre	l <sub>x</sub>	$\phi_{\sf b} M_{\sf sx}$	$\phi_{\rm b}M_{\rm bx}$	$\phi_v V_{vx}$	$\phi_{\rm c} N_{\rm s}$	$\phi_{c} N_{c}$	$\phi_t N_t$	$\phi_{\sf b} M_{\sf sxf}$	N <sub>ex</sub>	Classi	Ication
	kg/m	10 <sup>6</sup> mm <sup>4</sup>	kNm	kNm	kN	kN	kN	kN	kNm	kN	Australia	New Zealand
Stud Height 2440 mm												
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	60.7	86.7	3.16	144	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	38.7	70.4	2.67	107.9	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.87	40.2	29.0	61.9	2.45	89.6	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	18.7	44.2	1.76	71.1	SC	SC
Stud Height 2740 mm												
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	58.0	86.7	3.16	114	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	36.9	70.4	2.67	85.6	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.9	40.2	27.5	61.9	2.45	71.1	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	17.9	44.2	1.76	56.4	SC	SC
	Stud Height 3040 mm											
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	55.0	86.7	3.16	92.7	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	34.8	70.4	2.67	69.5	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.9	40.2	25.9	61.9	2.45	57.7	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	17.0	44.2	1.76	45.8	SC	SC



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#### Wall Stud Design Assumptions

Effective Lengths for Design								
Stud Height (mm)	2440	2740	3040					
No. of Noggings	1	1	2					
L <sub>ex</sub> (mm)	1952	2192	2432					
L <sub>ey</sub> (mm)	600	600	600					
L <sub>ez</sub> (mm)	600	600	600					

#### NOTES:

- 1. Noggings are equally spaced.
- 2. Lateral restraint is assumed to be provided the cladding.
- 3. Both flanges of the stud are restrained by the top and bottom plates, the nogging, and the cladding
- 4. Effective length  $L_{\text{ex}}$  is taken as 80% of the ength of the stud in accordance with NASH Handbook Clause 3.4.2.
- 5. Effective lengths  $L_{ev}$  and  $L_{ez}$  are assumed to be as per the table above.
- 6. No allowance has been made for holes in the web of the stud.

Symbol	Description					
I <sub>x</sub>	second moment of area about the major principal x-axis					
$\phi_{c} N_{s}$	design section capacity of a member in compression					
$\phi_{c} N_{c}$	design member capacity of a member in compression					
$\phi_{\rm b} M_{\rm sx}$	design section moment capacity about the x-axis					
$\phi_{\sf b} M_{\sf bx}$	design member moment capacity about the x-axis					
φ <sub>b</sub> M <sub>sxf</sub>	design yield moment capacity about the x-axis					
$\phi_{\rm v} V_{\rm vx}$	design shear capacity of the cross-section perpendicular to the x-axis					
N <sub>ex</sub>	elastic buckling load about the major principal x-axis					
$\phi_t N_t$	design section capacity of a member in tension					
L <sub>ex</sub>	effective length for buckling about the major principal x-axis					
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis					
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis					

#### References

AS/NZS 4600 Cold-Formed Steel Structures.

NASH Standard (NZ), Residential and Low-Rise Steel Framing, Part 1: Design Criteria. NASH Standard (Aust.), Residential and Low-Rise Steel Framing, Part 2: Design Solutions. NASH Handbook (Aust.), Best Practice for Design and Construction of Residential and Low-Rise Steel Framing, Chapter 3.

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#### Table 7.3



# WALL PLATE DESIGN CAPACITIES



	Mass			NA	SH							
Designation	per		Full Lipped Chan	nel (at midspan	ı)	C	Channel Lips Rem	Wall	Plate			
Designation	metre	l <sub>y</sub>	$\phi_{c}N_{c}$	$\phi_{\sf b}  M_{\sf byL}$	$\phi_{\rm b}  M_{\rm byW}$	$\phi_c N_s$	$\phi_{\sf b} M_{\sf syT}$	$\phi_{\sf b} M_{\sf syW}$	$\phi_v V_{vy}$	Classi	lication	
	kg/m	10 <sup>6</sup> mm <sup>4</sup>	kN	kNm	kNm	kN	kNm	kNm	kN	Australia	New Zealand	
89 x 41 x 1.55 LCN - G450	2.18	0.0584	68.6	0.804	0.856	61.4	0.400	0.470	27.4	PC	PD	
89 x 41 x 1.15 LCN - G500	1.64	0.0450	44.1	0.590	0.579	39.5	0.265	0.352	23.1	PB	PC	
89 x 41 x 0.95 LCN - G550	1.36	0.0378	33.4	0.486	0.509	30.2	0.205	0.277	21.2	PB	PC	
89 x 41 x 0.75 LCN - G550	1.08	0.0304	21.2	0.345	0.287	18.7	0.129	0.176	14.9	PA	PA	

NOTES:

1. The capacities for the full lipped channels are based on an effective length  $L_e = 0.6$  m.

2. The capacities of channels with lips removed are section capacities.

3. No allowance has been made for holes in the web of the plate in the determination of  $I_{y}$ .

4. The NASH Classifications are based on the capacities of the full lipped channels.

5. The second moment of area  $I_{\rm v}$  for the full lipped channel is used for the NASH Australia classification.

	Symbol	Description
	l <sub>y</sub>	second moment of area about the minor principal y-axis
	$\phi_{\rm c} N_{\rm s}$	design section capacity of a member in compression
	$\phi_{c} N_{c}$	design member capacity of a member in compression
	$\phi_{\sf b} M_{\sf byL}$	design member moment capacity about the y-axis (lips in compression)
	$\phi_{\rm b} M_{\rm byW}$	design member moment capacity about the y-axis (web in compression)
	$\phi_{\sf b}M_{\sf syT}$	design section moment capacity about the y-axis (toes in compression)
vi	$\phi_{\sf b}M_{\sf syW}$	design section moment capacity about the y-axis (web in compression
	$\phi_{v} V_{vy}$	design shear capacity of the cross-section perpendicular to the y-axis
	L <sub>e</sub>	effective length ( $L_{ex} = L_{ey} = L_{ez}$ )



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# Appendix A: SIGNATURE CURVES

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### GENERAL

This appendix provides the signature curves for each of the sections contained in these Design Capacity Tables. The signature curves were produced in the Thin-Wall buckling analysis program developed by The University of Sydney, and form the basis of design using the Direct Strength Method (DSM). They are included here to provide a clear picture of the buckling behaviour of the sections under the following loading conditions:

axial compression

bending about the x-axis

bending about the y-axis (lips in compression)

bending about the y-axis (web in compression)



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